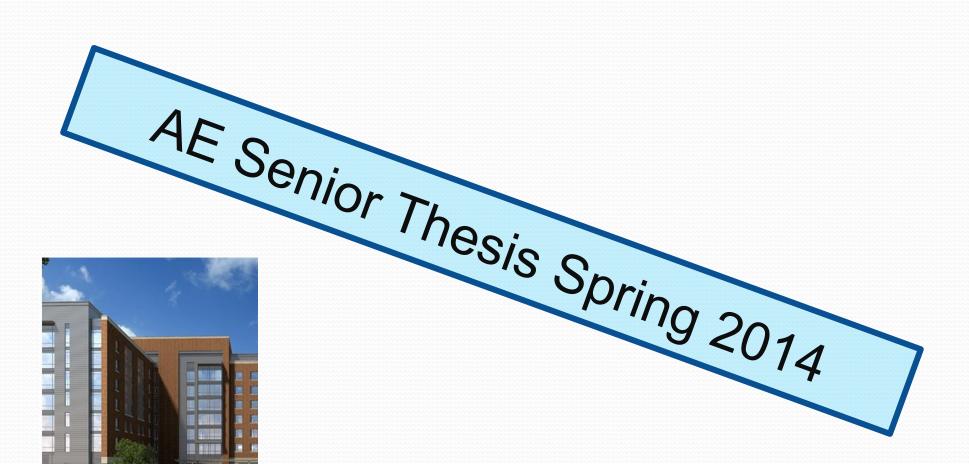


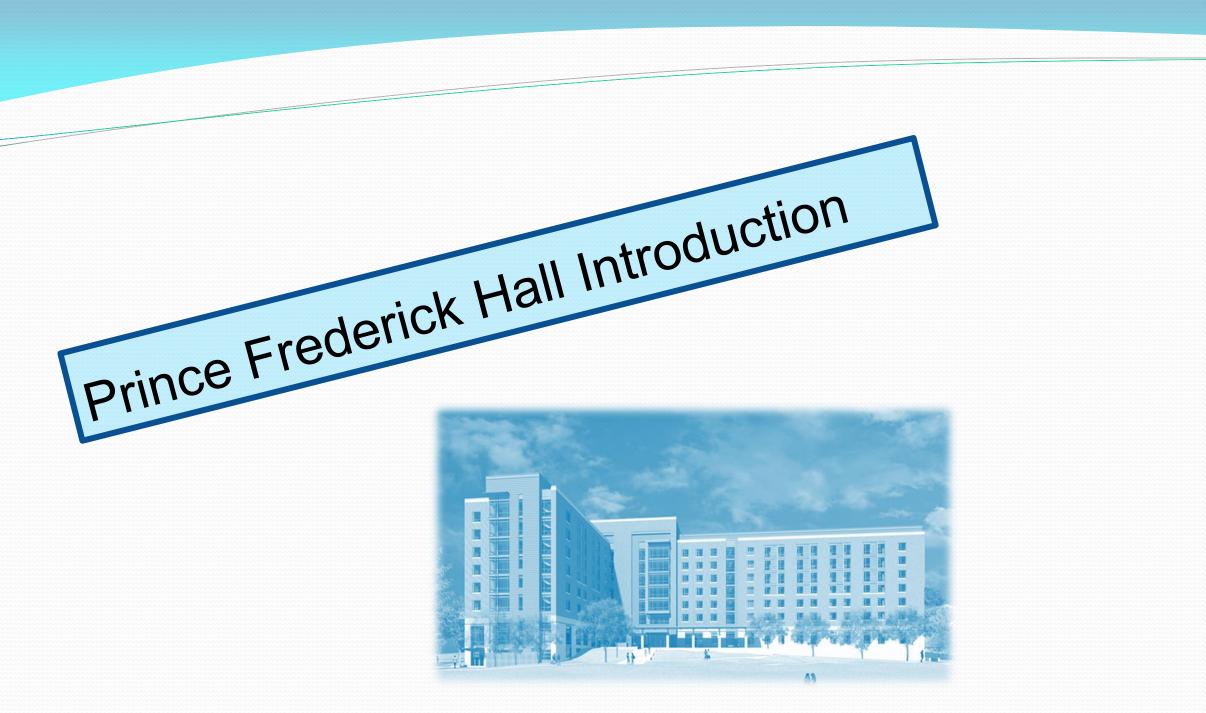
Advisor: Professor Sustersic





Prince Frederick Hall University of Maryland College Park, MD





Building Statistics

- Multi-purpose Dormitory
- 185,000 gSF
- 7 Stories Above Ground/ 1 Underground •
- Gravity System: Two Way Concrete Slabs w/ Concrete Columns
- Lateral: Ordinary Concrete Shear Walls

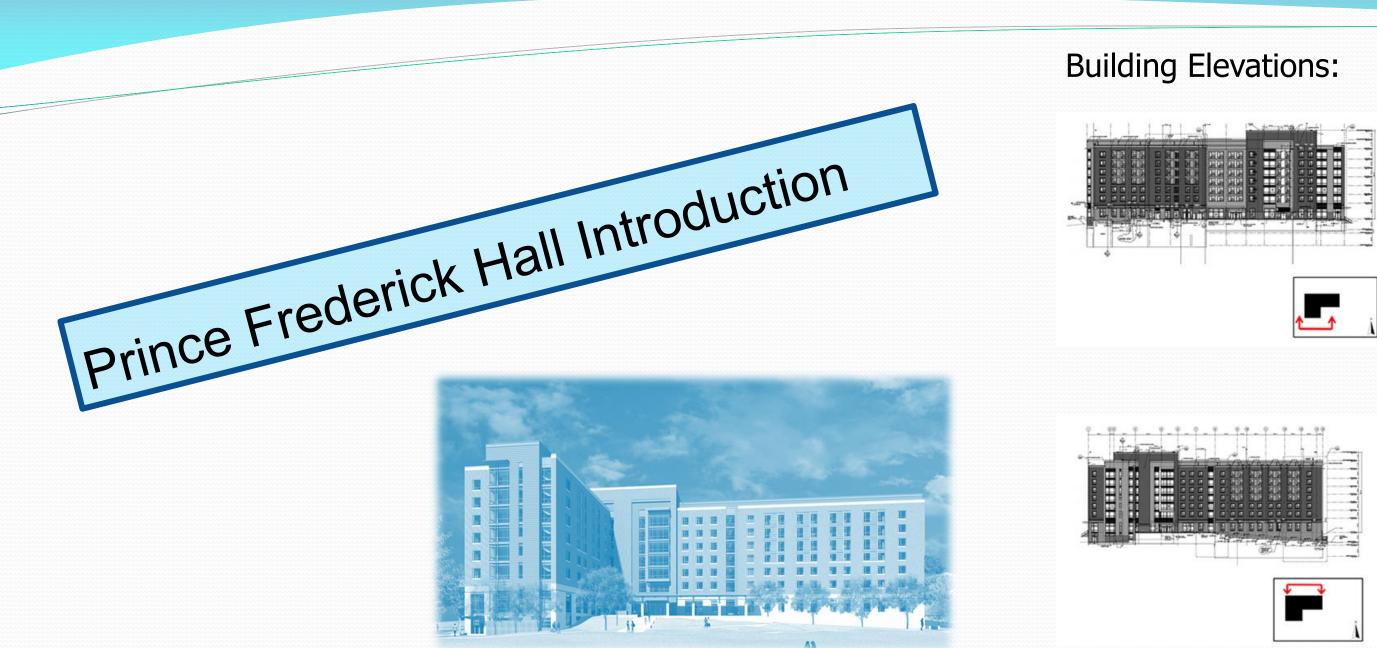
Project Team

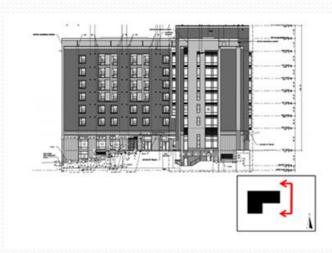
- Architects: WDG Architecture
- Contractor: Clark Construction
- Civil Engineers: Site Resources Inc.
- Structural Engineers: Cagley & Associates

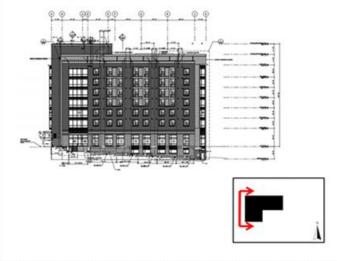




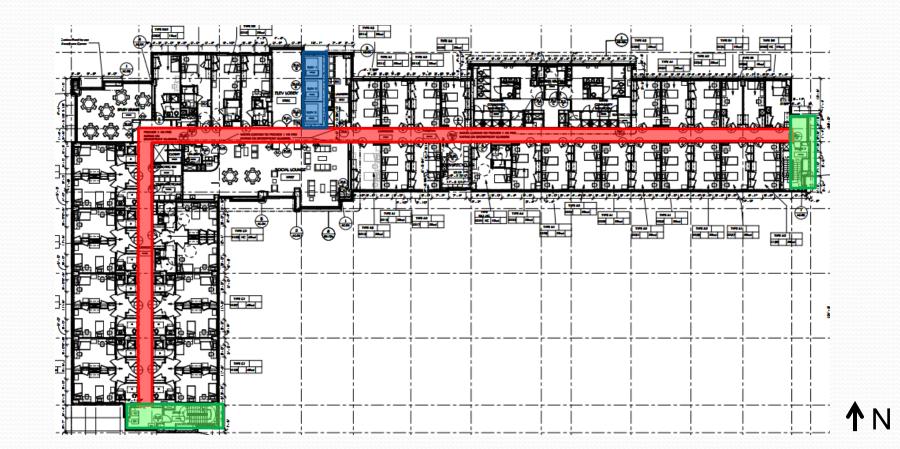




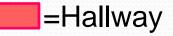




Typical Floor 2-7 Plan:



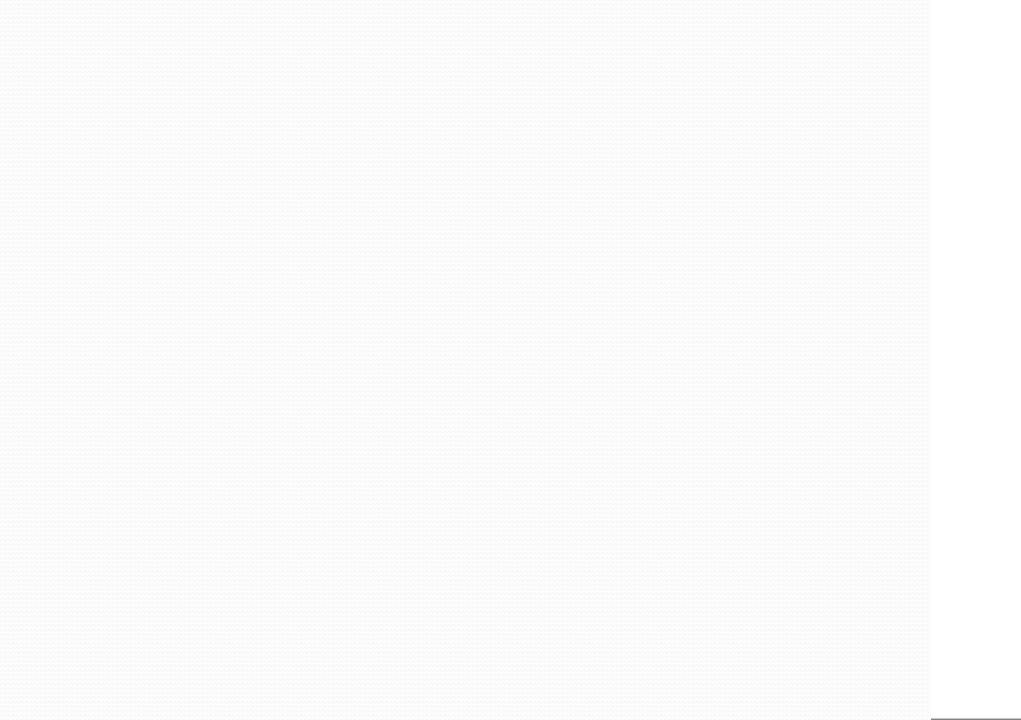


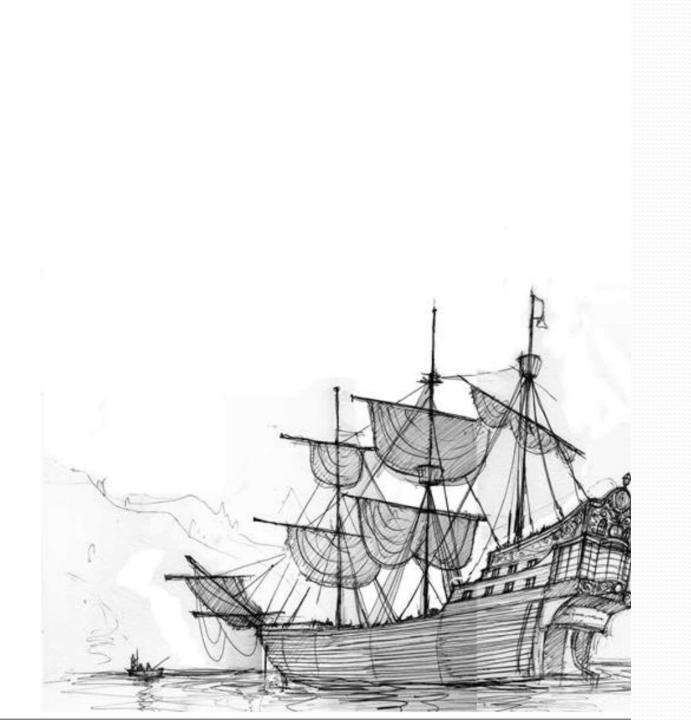






Blackbeard's Oasis Indoor Water Park and Hotel



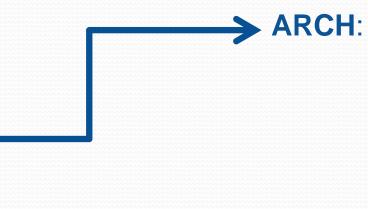




Design a brand new Luxury Family Resort:

With on site Entertainment

Luxury Accommodations









Structural Design Water Park

Structural Design: Hotel

3. Design Water Park Floor Plans

STRUC:





- 1. Pick New Site
- 2. Design New Floor Plans Hotel



1. Design Water Slide Structure

2. Design Water Park Gravity/Lateral Systems

3. Re-design Hotel Gravity/Lateral Systems





Hotel Information

- Hotel Size: 185,000 gSF
- Stories: 7 stories, 1 underground

Introduction Blackbeard's

- 234 Guest Rooms
- Arcade

Problem Statement

Bar/Night Club





Indoor Water Park Information

- Indoor Water Park: 45,000 gSF
- Stories: 4 stories tall
- Over 10 Water Slides and Attractions
- Large 120,000 Gallon Wave pool
- Thrilling Speed Slides

Structural Design: Hotel

Structural Design Water Park





new site:

Arundel Mills Circle Hanover, Maryland



Problem Statement

Introduction Blackbeard's **Architectural Design**





Arundel Mills Mall

Maryland Live! Casino

Costco / Walmart

Stand Alone Restaurants

Structural Design: Hotel

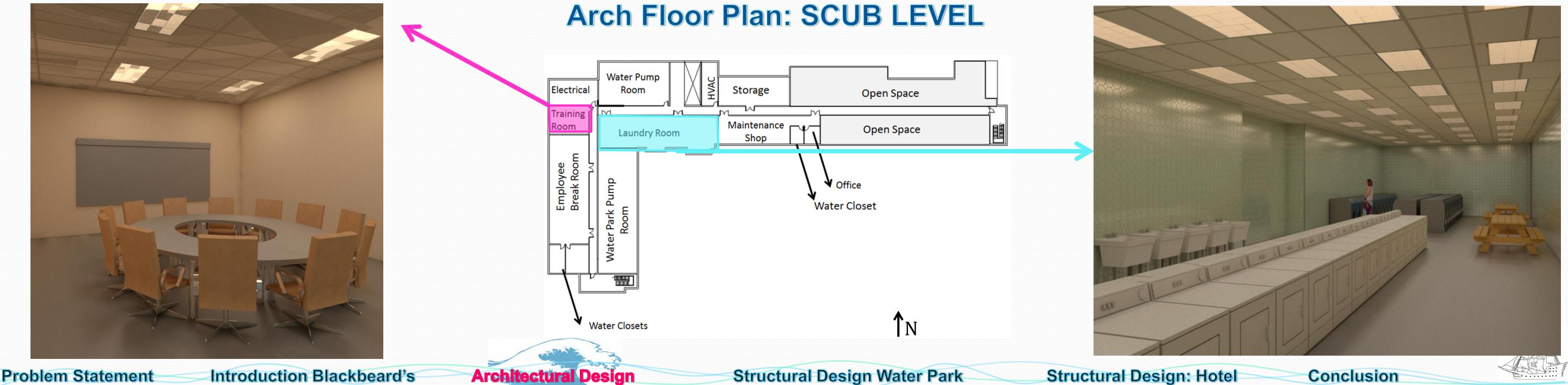
Structural Design Water Park



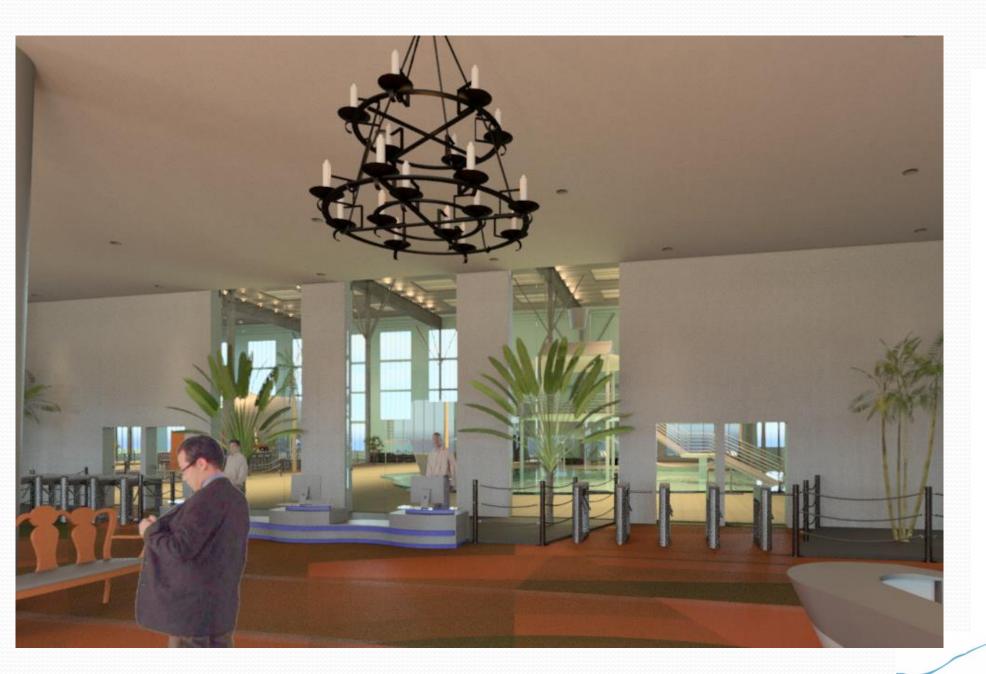
- Awesome Shopping
- Diverse Dinning
- Entertainment
- Casino Gambling
- Prime Location



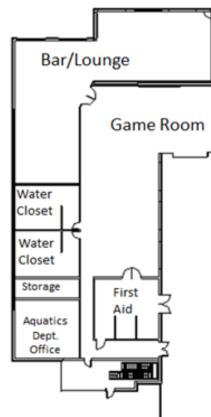




Structural Design: Hotel

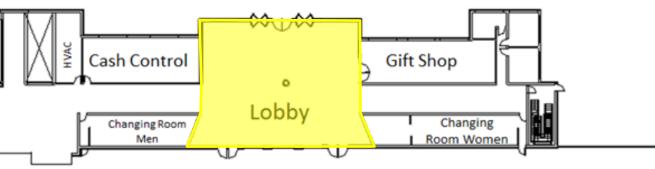


Arch Floor Plan: First Floor Plan



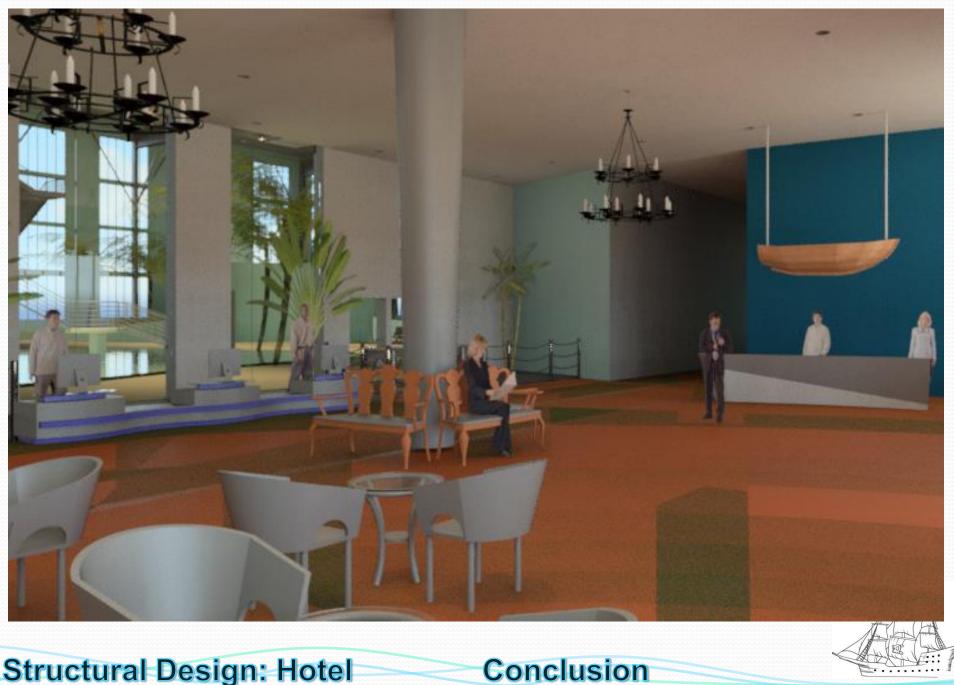
Problem Statement Introduction Blackbeard's

Architectural Design



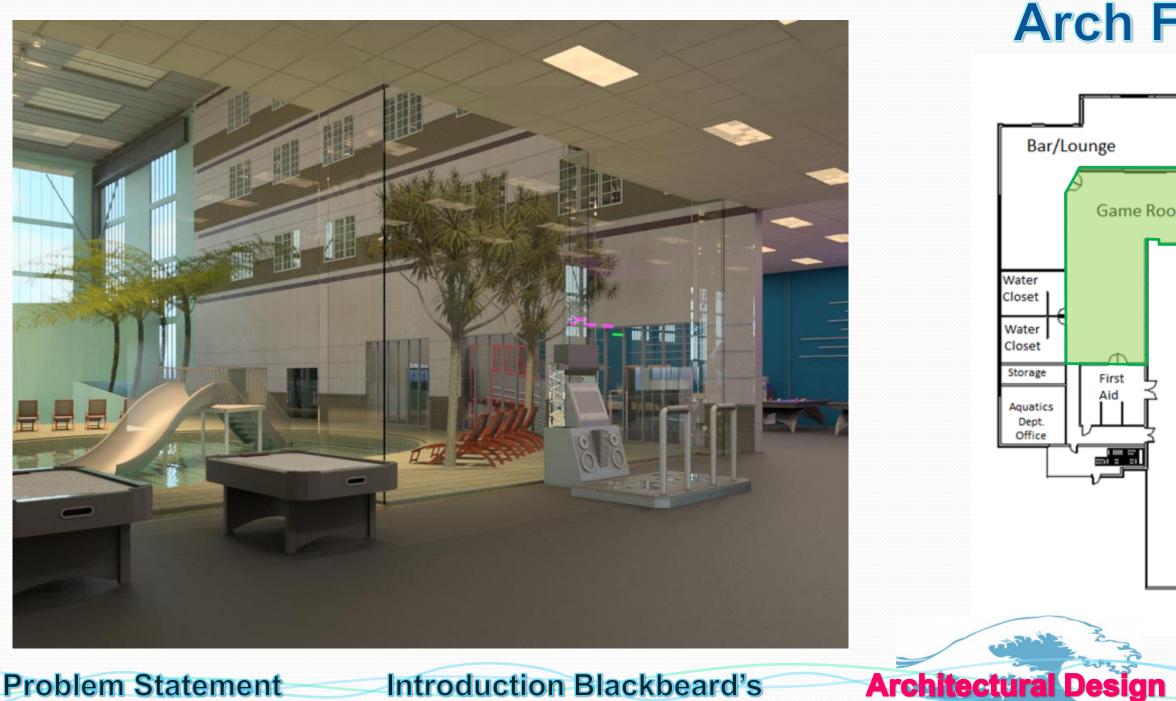
Indoor Water Park

1N

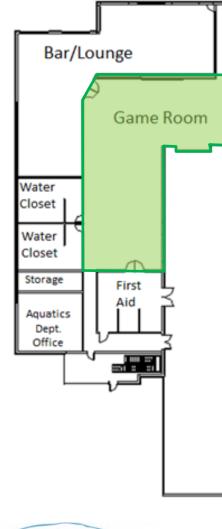


Structural Design Water Park

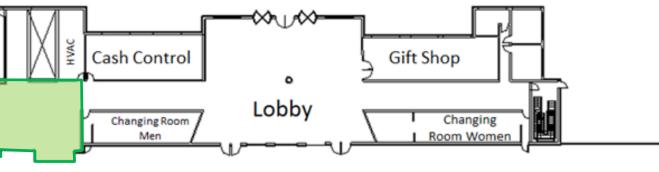
Structural Design: Hotel







Arch Floor Plan: First Floor Plan

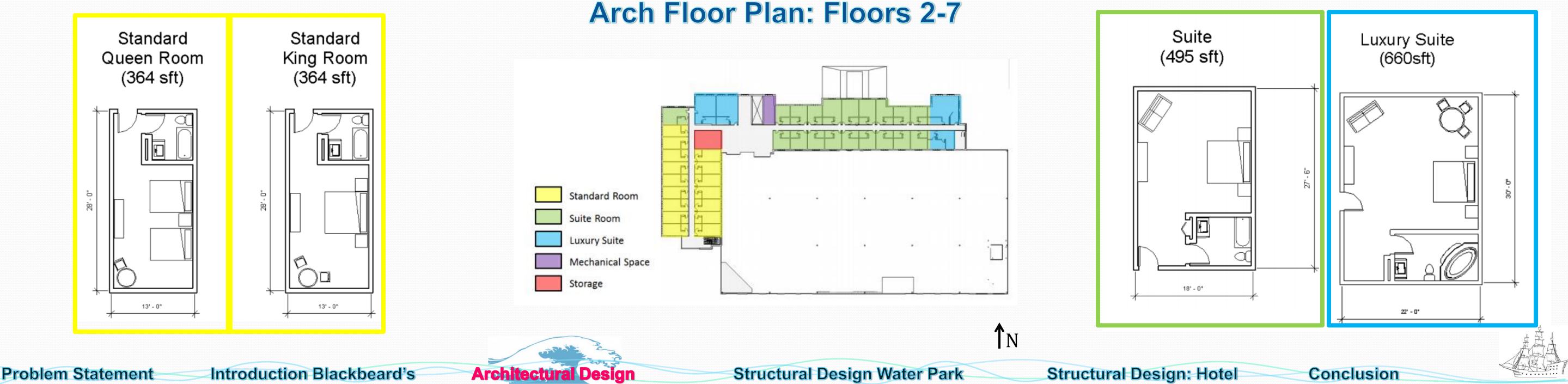


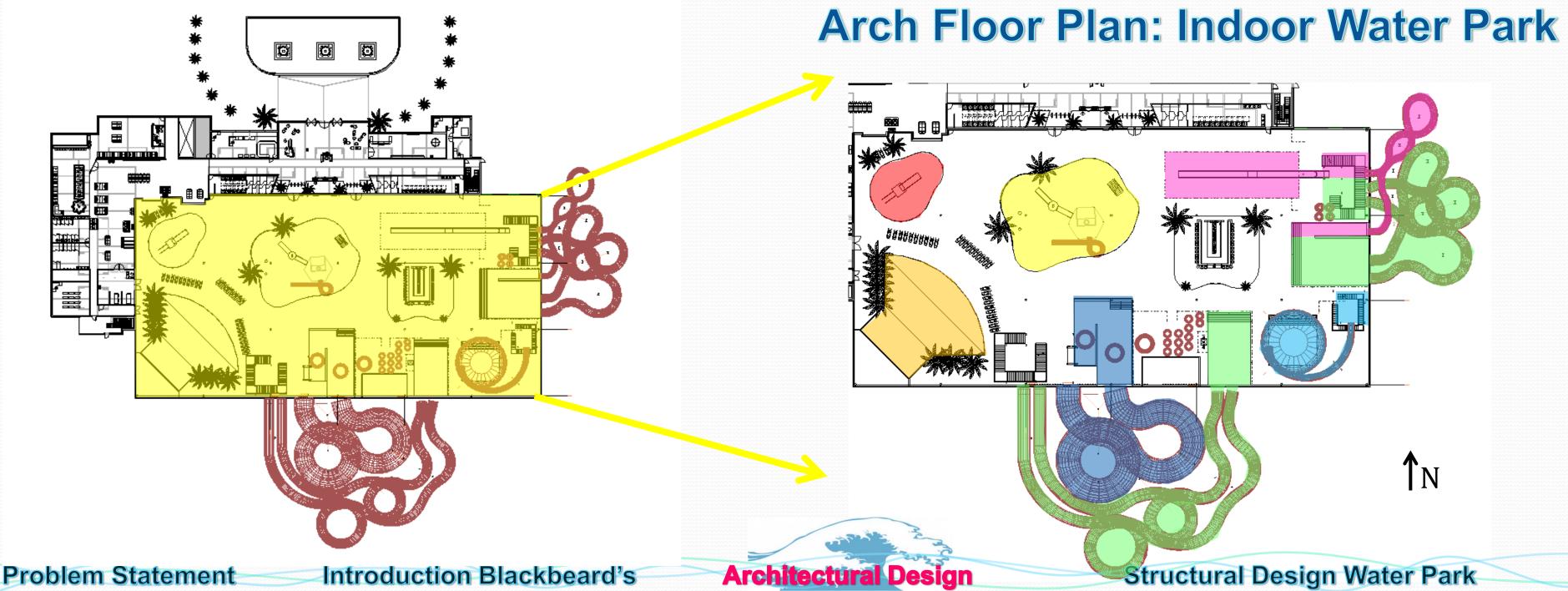
Indoor Water Park



Structural Design: Hotel

Structural Design Water Park



















Structural Design: Hotel

Family Splash Tower

Racing Tube Slides





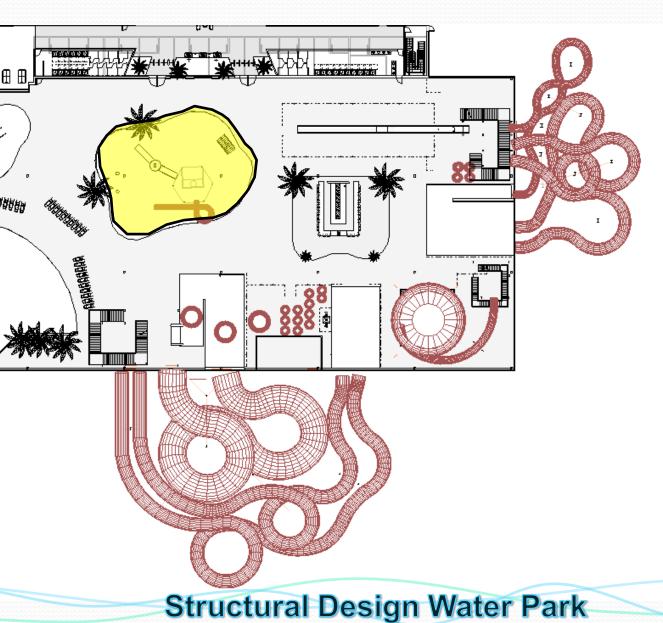




Introduction Blackbeard's **Problem Statement**

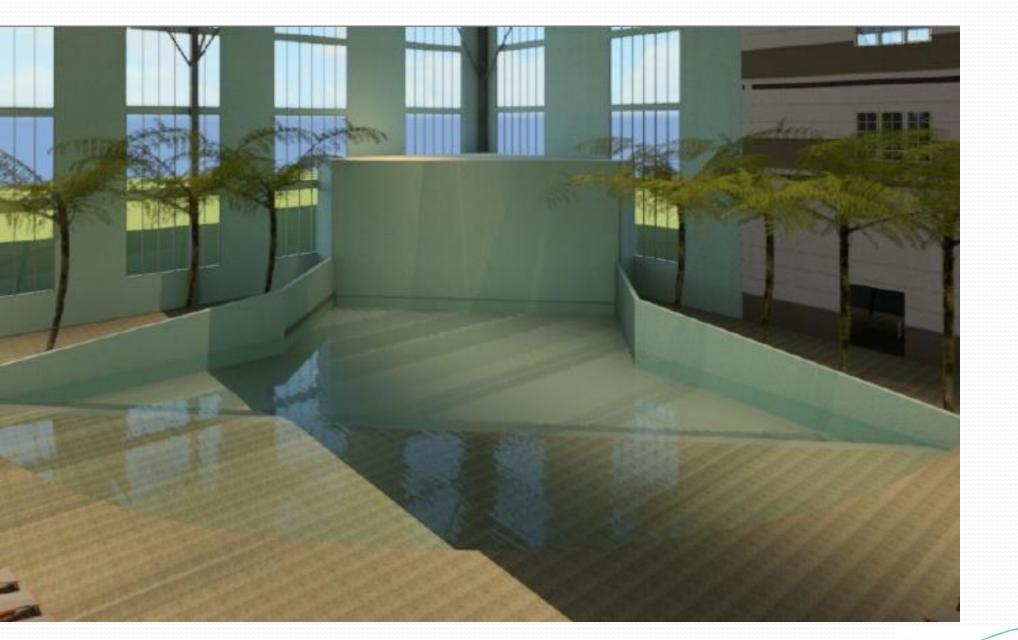
Architectural Design

Family Splash Tower

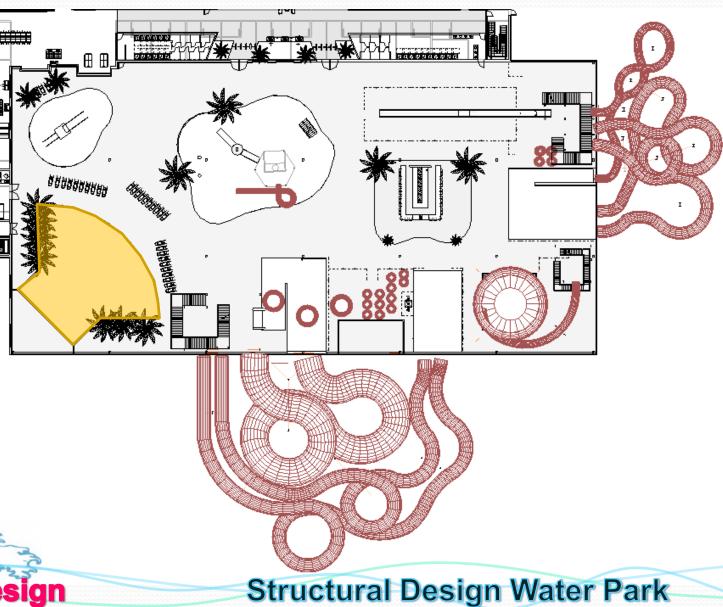




Structural Design: Hotel







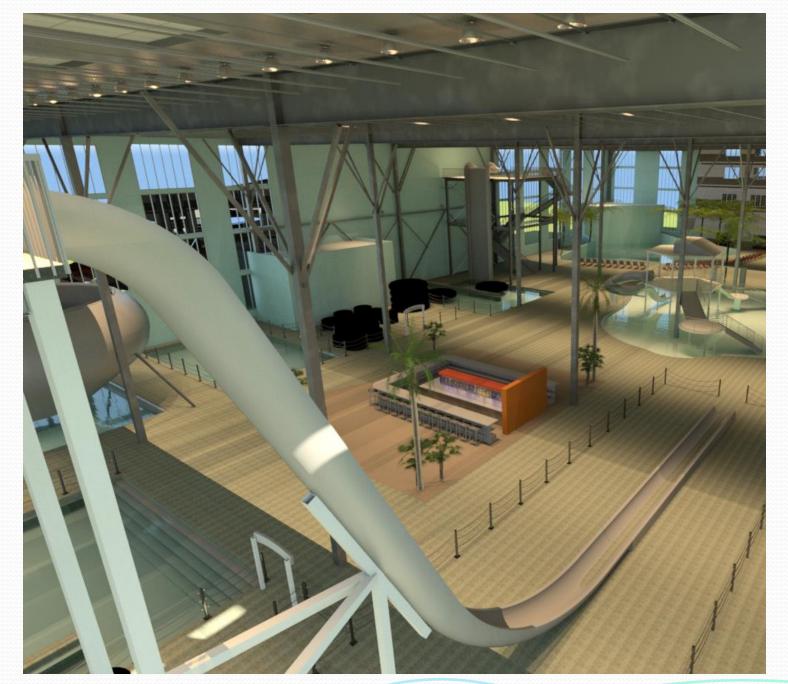


Blue Lagoon Wave Pool

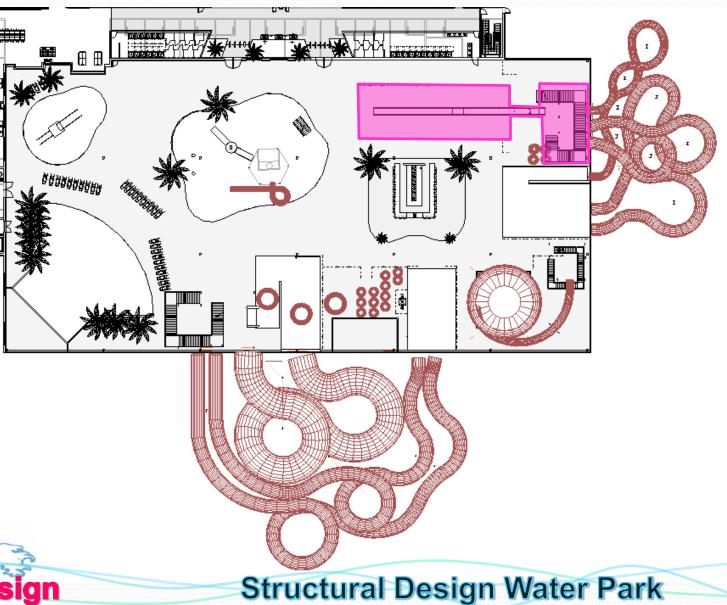


Structural Design: Hotel

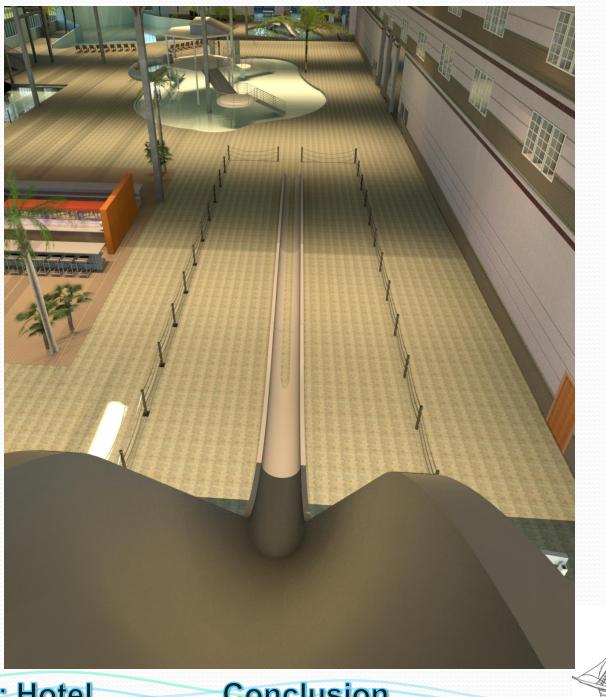








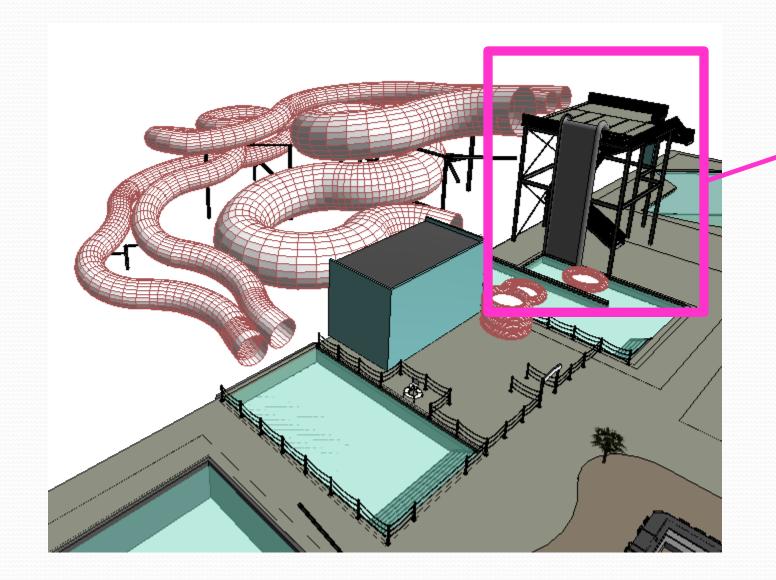
Free-FALL (Speed Slide)

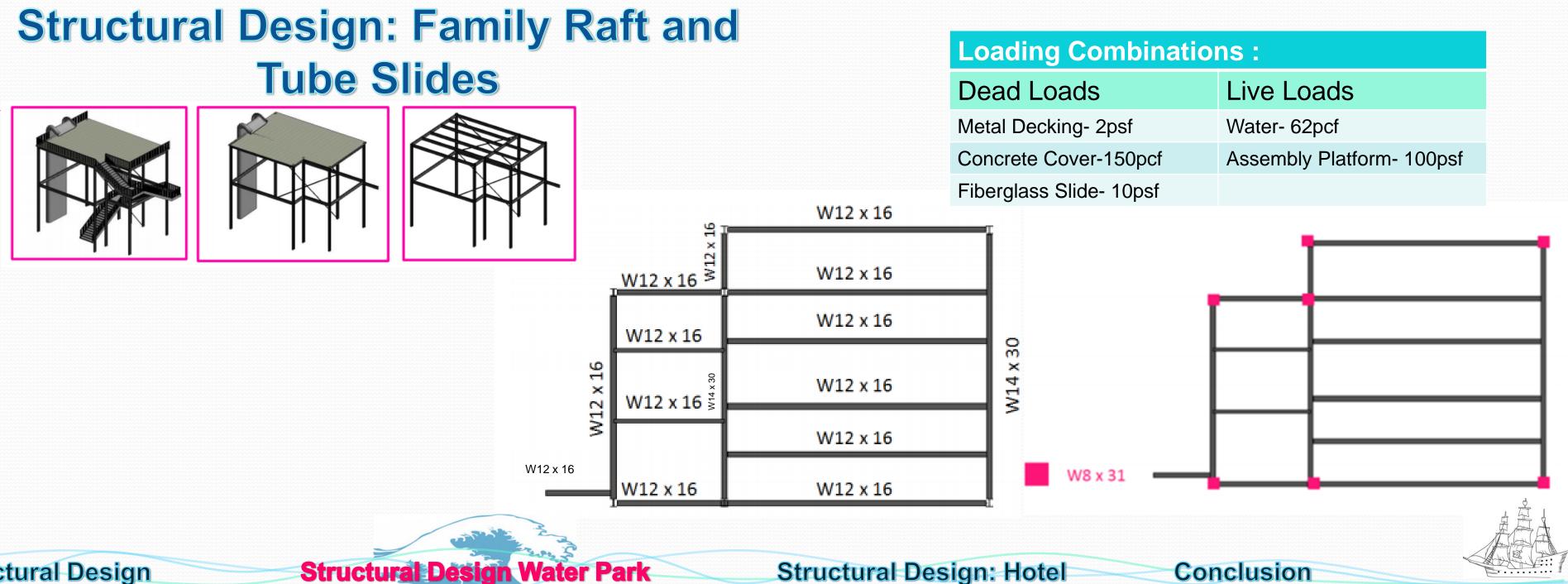


Structural Design: Hotel

Conclusion

and the second s

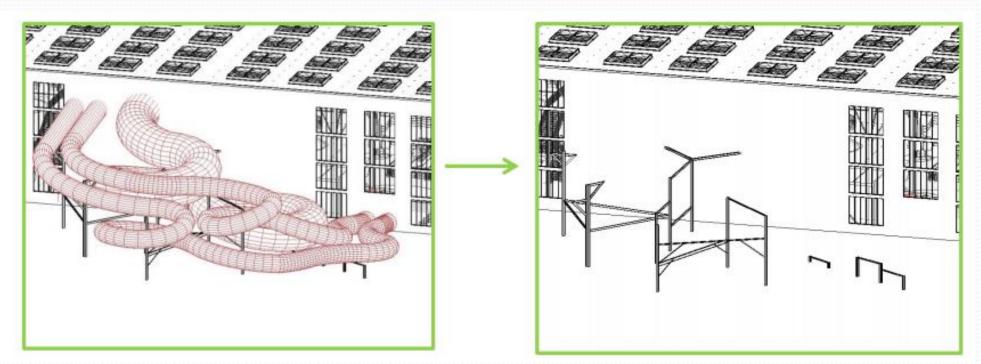






Loading Combinations:

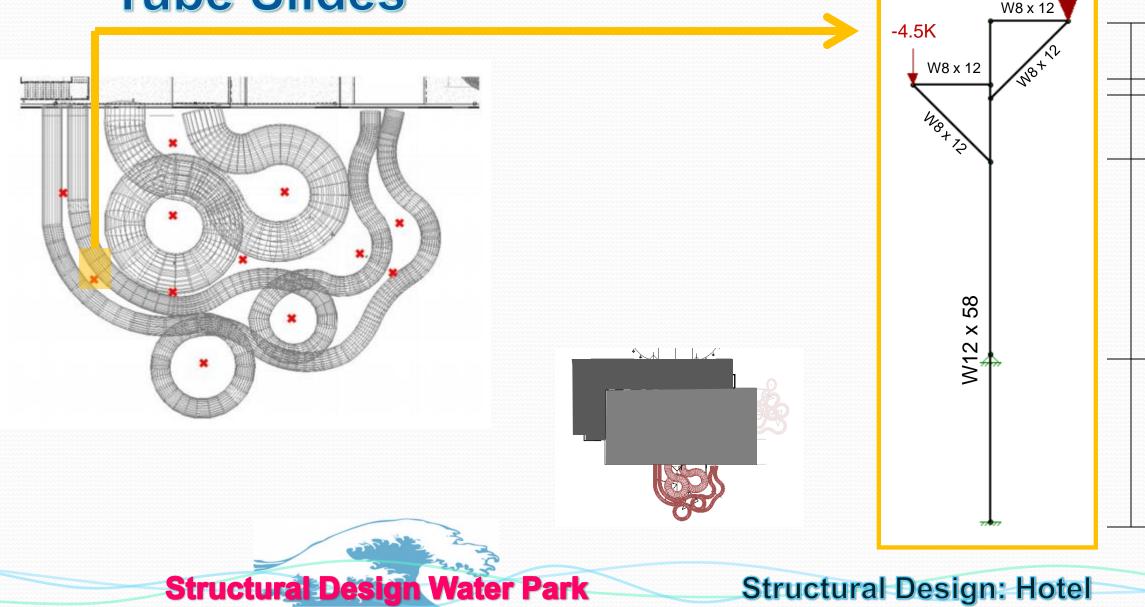
- Designed with ASTM F2376-06 Loading Combinations
- Normal Building Codes Generally Do Not Apply
- Dead Load+ Rider Load + Water Load
- Wind Load Does Not Control (X1.4 Section 6)
- Assume Worst Case Scenario



Problem Statement Introduction Blackbeard's

Architectural Design

Structural Design: Family Raft and Tube Slides



Loading Combinations

Two Riders Same Location

One Rider Left

One Rider Right

No Water Left/ Rider Right

Rider Left / No Water Right

39'

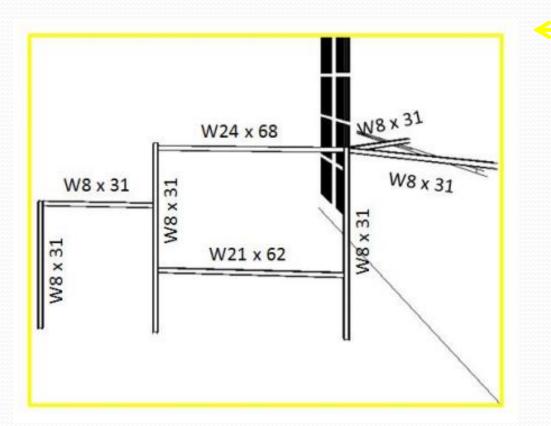
15'

13'

-9.8K



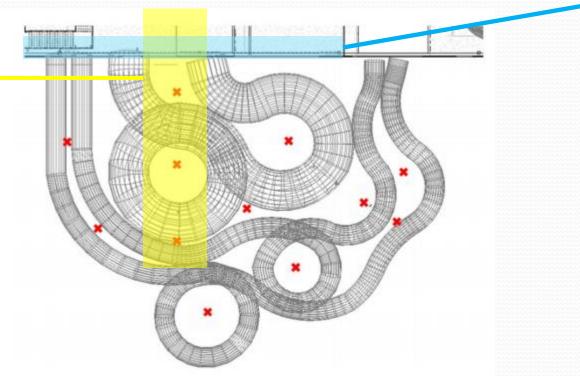
- Higher Loads From 14' Diameter Family
 Raft
- Too Heavy for previous column design
- Designed a No-Sway Frame

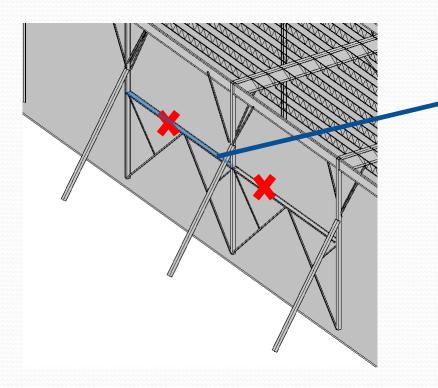




Structural Design: Family Raft and Tube Slides

Structural Design Water Park

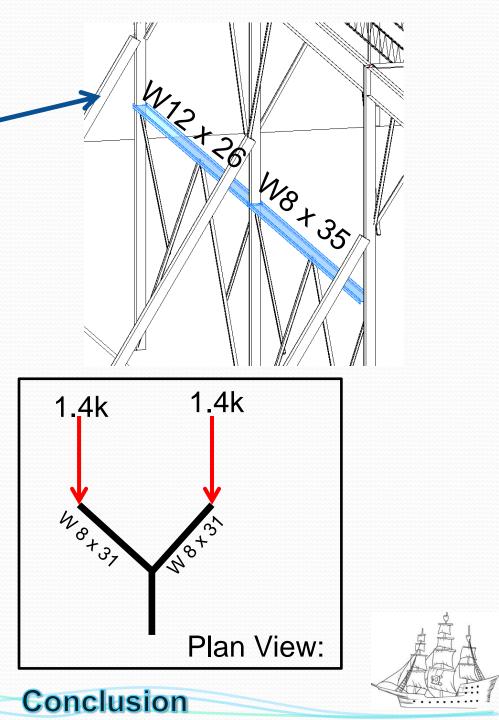




 W8x31 designed as tension members/ checked for compression

WS Structure Applies a 1.4
 K load to tie back

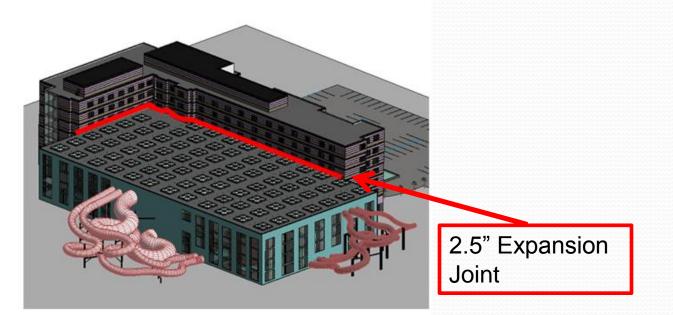
Structural Design: Hotel



Roof Conditions:

Expansion Joint: Sized off of Max Deflections of both structures the 5th floor.

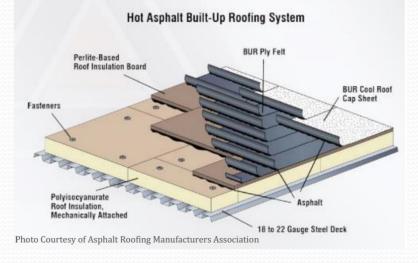
2.5" Roof to Wall System



Architectural Design

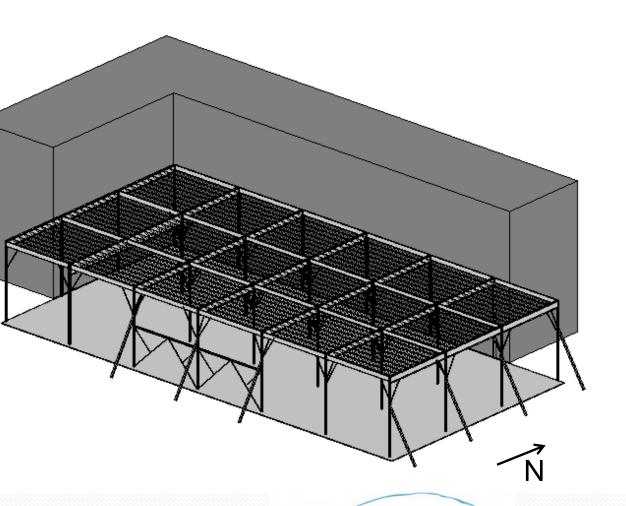
Built Up Roof:

Problem Statement



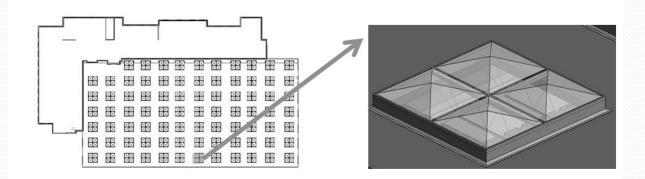
Introduction Blackbeard's

Structural Design: Water Park Gravity System



Structural Design Water Park

Skylights:



Loading Conditions:

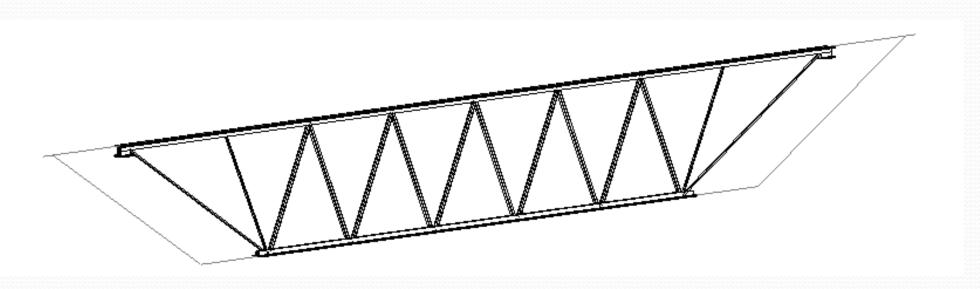
Metal Decking- 2psf Rigid Insulation- 2 psf Built Up Roof- 20psf HVAC/ MISC -12psf Skylights- 6psf Ordinary flat roof live – 20 psf Snow Flat Projection- 22 psf

Structural Design: Hotel



Joist Design:

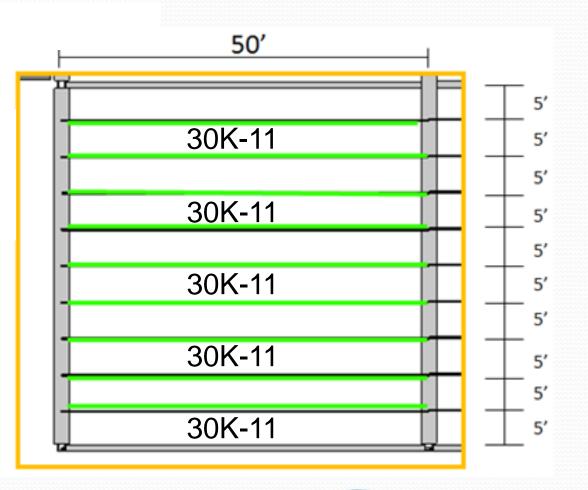
- Economy K-Series Tables Were Used
- 50 Foot Spans
- Trib Width 5 Feet
- No Depth Constraints



Problem Statement Introduction Blackbeard's



Structural Design: Water Park Gravity System



Structural Design Water Park

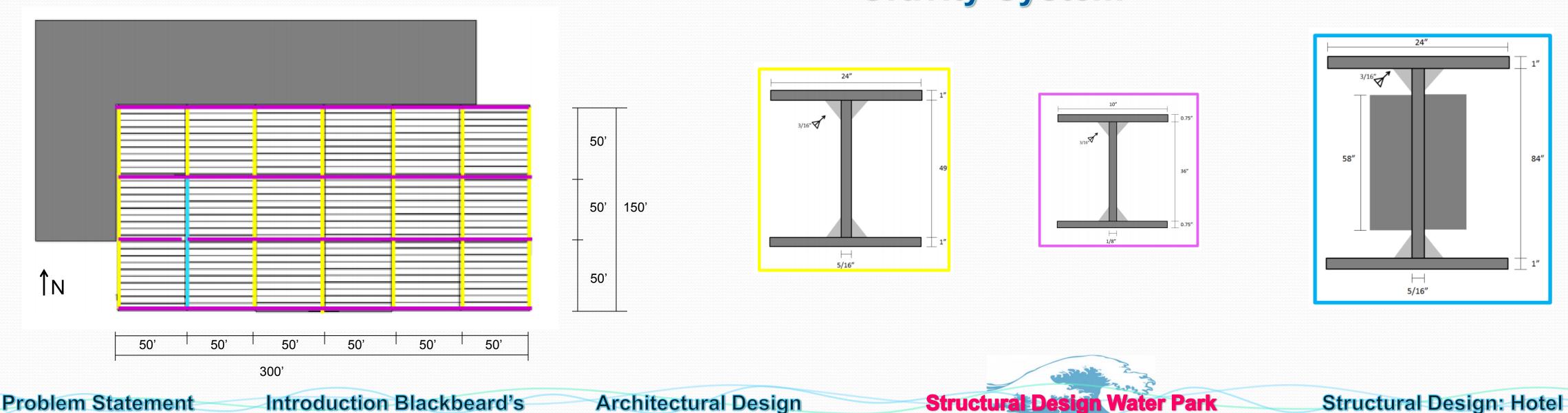
Structural Design: Hotel

		-
 	-	-
 	-	
 		-
 		-
		-
-		
 -		
 -		
 		-



Structural Design: Water Park Gravity System

Plate Girder Layout





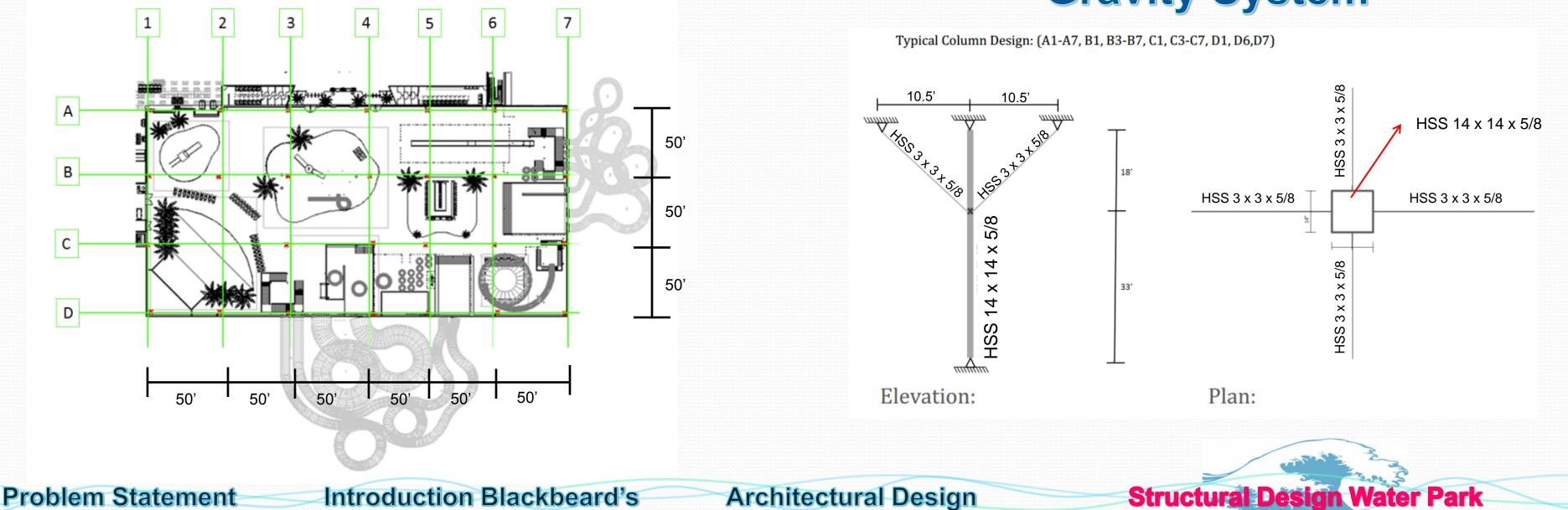
- Depth of beam (Guess and Check)
 - L/D= 10 to 12
- \circ Checked for a Slender Web
- Checked for Shear Strength
- Weld Shear Flow was compared to shear yielding and shear rupture.





Structural Design: Water Park Gravity System

Column Layout



- Open Layout Concept
- Large Unbraced Length
- Mold Growth From High Traffic
- Erosion From Chlorine

Epoxy Coating Used

Structural Design: Hotel



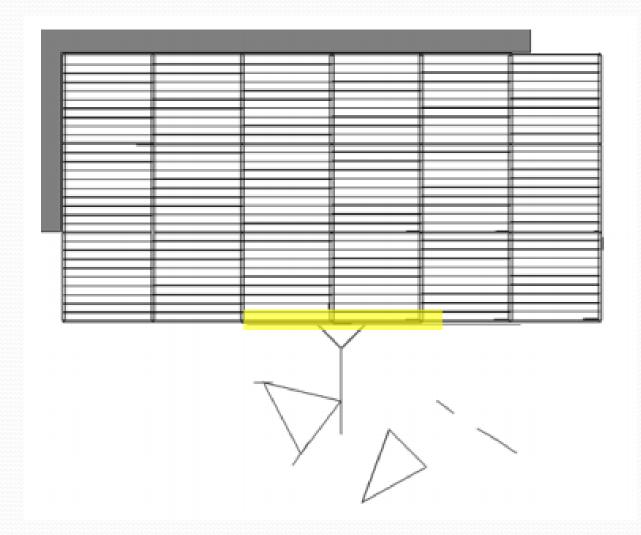
Relative Column Bracing Designed

HSS Hollow Structural Members Used





Water Slide Tie Back System

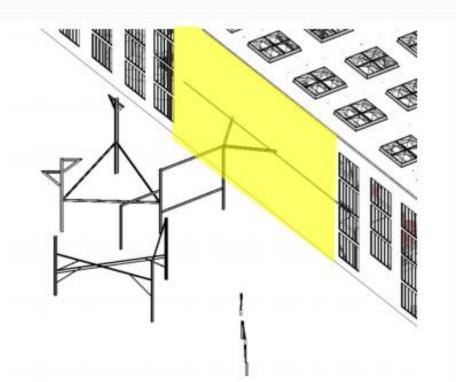


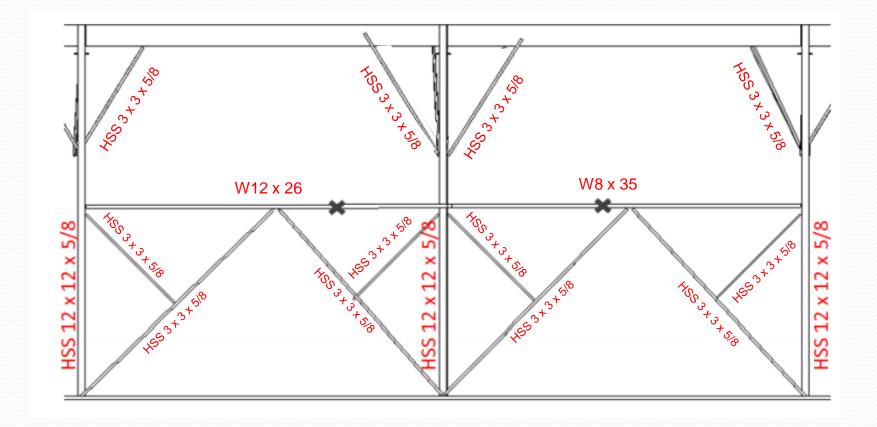
Problem Statement Introduction Blackbeard's

Architectural Design

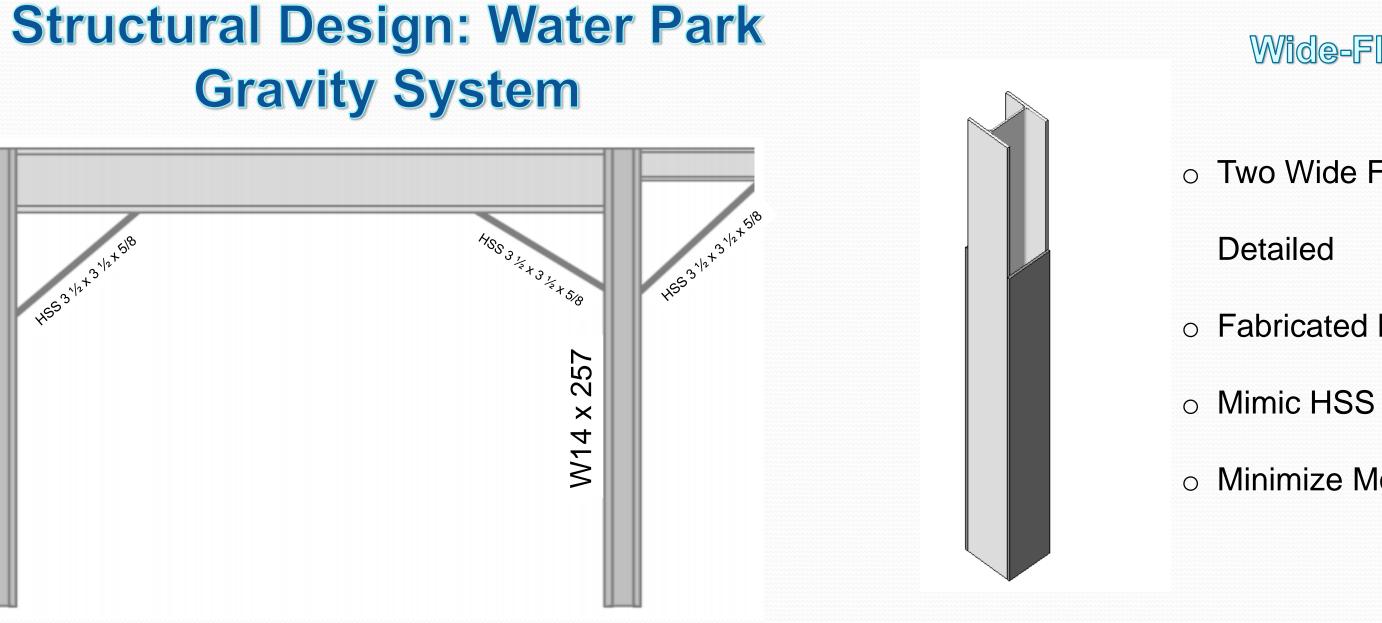
Structural Design: Water Park Gravity System

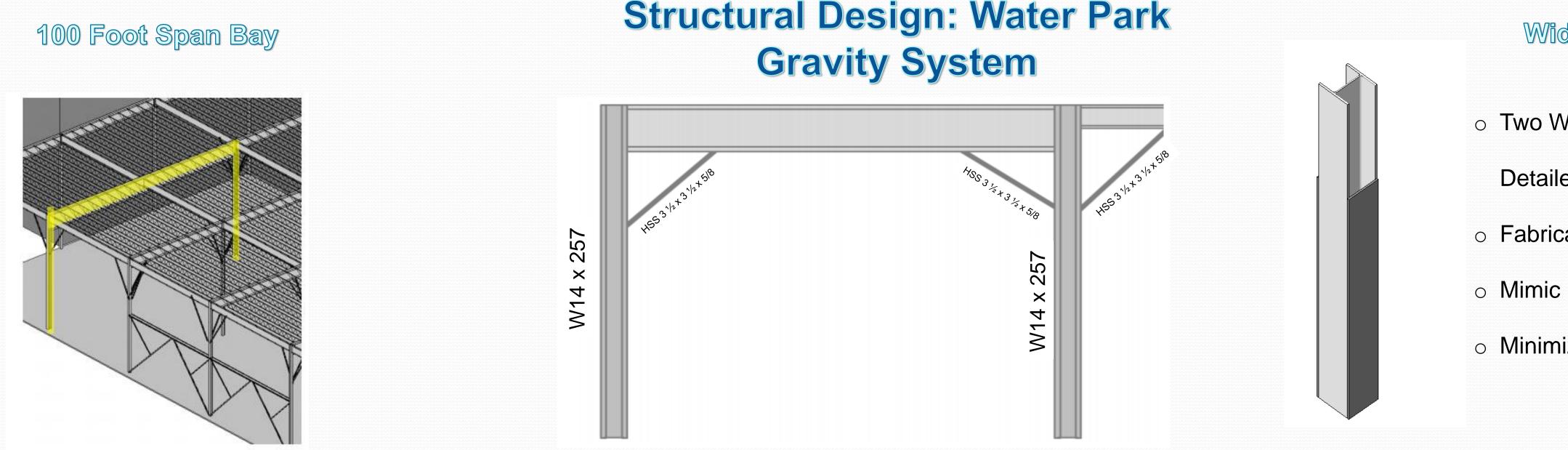
Structural Design Water Park





Structural Design: Hotel















• Two Wide Flange Columns

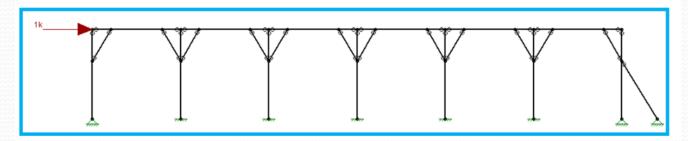
• Fabricated Before Installation

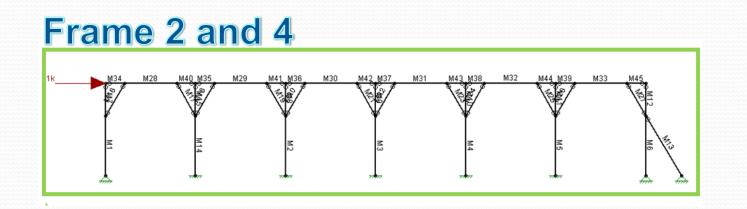
Minimize Mold Growth

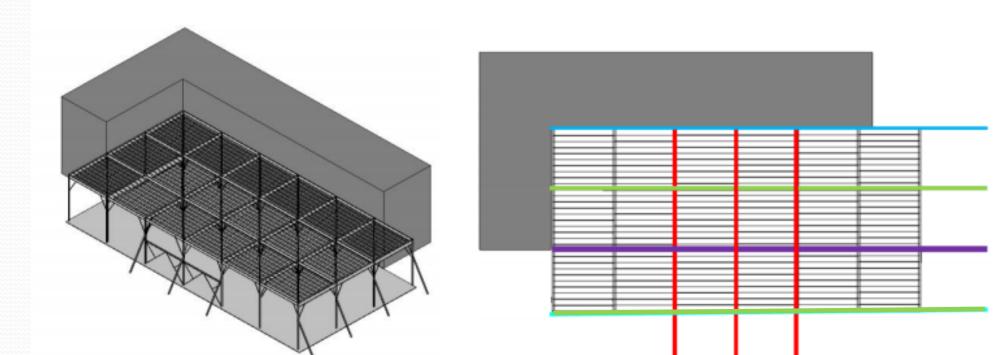


Frame 1







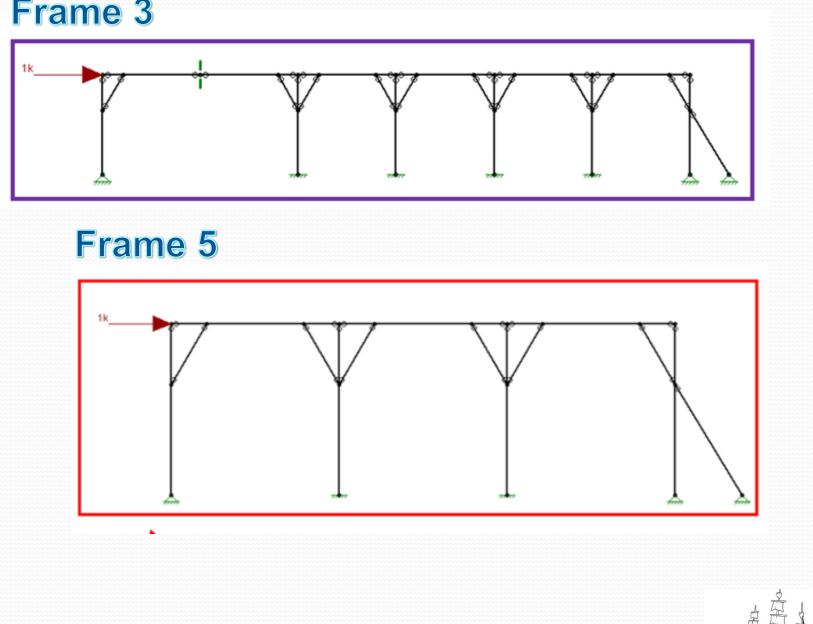


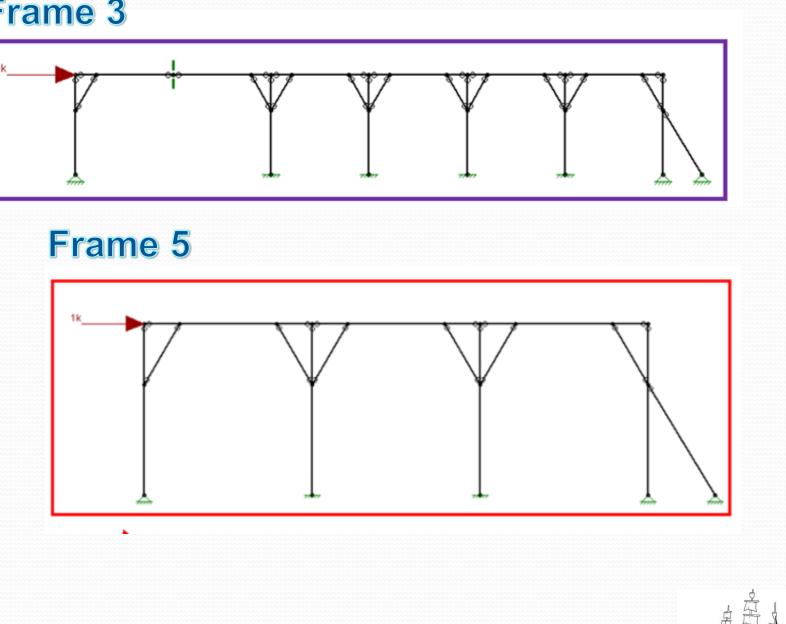




Structural Design: Water Park Lateral System

Frame 3



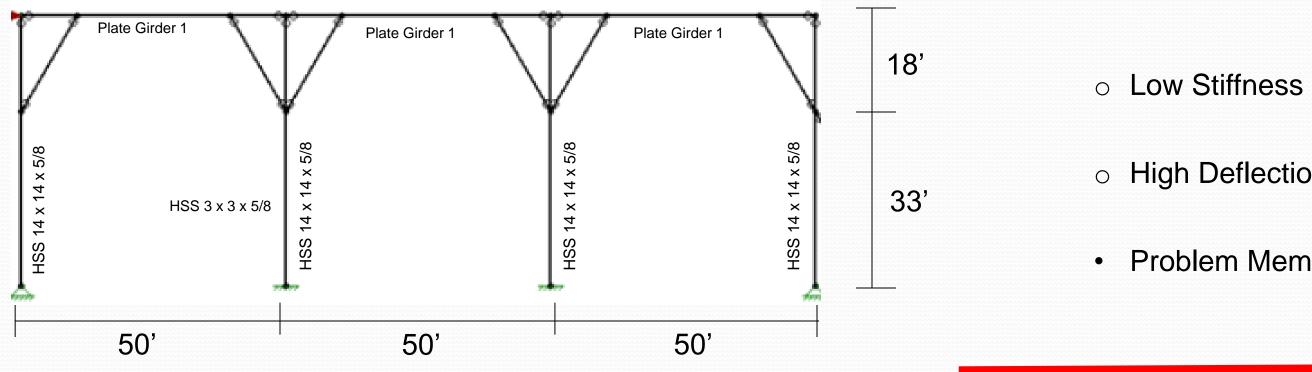






Structural Design: Water Park Lateral System

Original Frame 5:



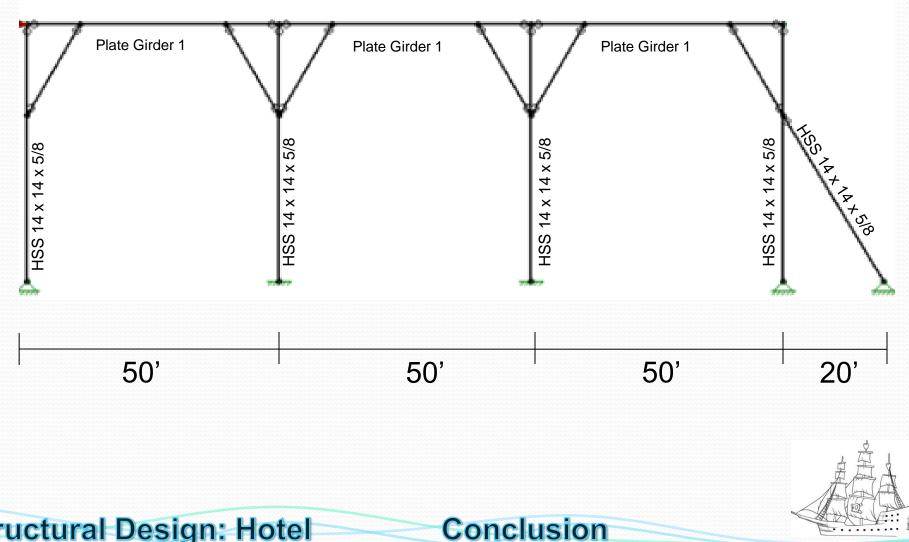
Problem Statement Introduction Blackbeard's



• High Deflection

Problem Members: Unbraced Portion of Columns

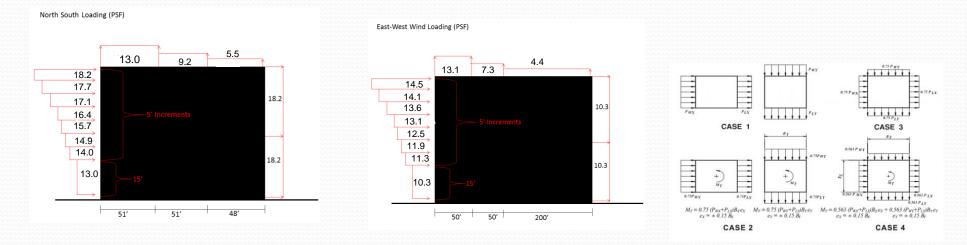
Structural Design Water Park



Structural Design: Hotel

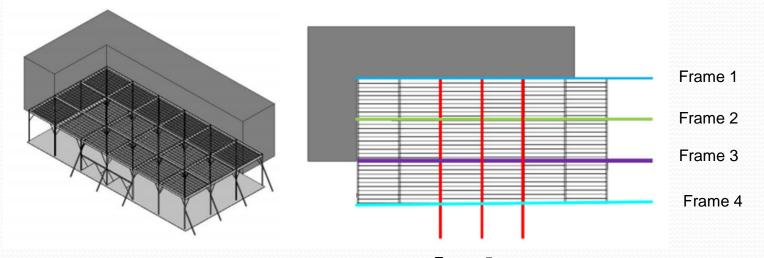
Wind Loading ASCE 7-10

Structural Design: Water Park Lateral System



Frame Deflection Due to Wind Loading Cases:

Loading Case	Frame With Largest Deflection	Max ∆ (In)	Max Allowable Δ (H/400)	Pass?
Case 1	Frame 5	0.70	1.53	Yes
Case 2	Frame 2	1.51	1.53	Yes
Case 3	Frame 5	0.4	1.53	Yes
Case 4	Frame 5	1.01	1.53	Yes



Problem Statement Introduction Blackbeard's

Architectural Design

Seismic Loading ASCE 7-10

Frame 5

Structural Design Water Park

80.8 Kips

80.8 Kips **4**095'k

Frame Deflection Due to Seismic Loading:

Loading Case	Frame With Largest Deflection	Max ∆	Allowable Deflection (in)	Pass?
Seismic	Frame 2	1.06	1.53	Yes

Structural Design: Hotel



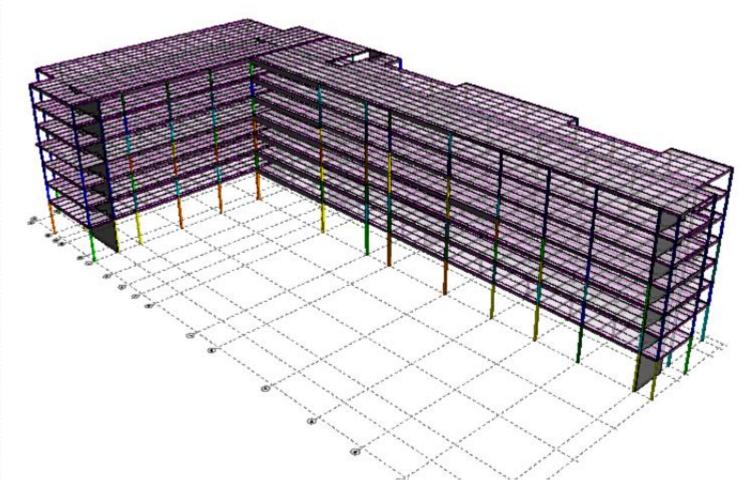






New Gravity Live Loads

Occupancy	Live Load (psf)	Partition (psf)	Total Load (psf)	Reducible?
Arcade	75	10	85	Yes
Bar	100	10	110	Yes
Bathroom	100	0	100	Yes
Corridor	100	0	100	No
Corridor(Above 1 st Floor)	70	0	70	No
Hotel Room	40	0	40	Yes
Hospital	40	10	50	Yes
Lobby-Assembly Room	100	0	100	Yes
Mechanical Space	150	0	150	No
Office	50	10	60	Yes
Retail	100	10	110	Yes
Roof	20	0	20	No



Structural Design Water Park

Problem Statement Introduction Blackbeard's



Structural Design: Hotel Gravity System

Composite Decking Instead of 2-Way Concrete Slabs :

- Superimposed Loading: 100psf
- 9 Foot Spans

Structural Design: Hotel

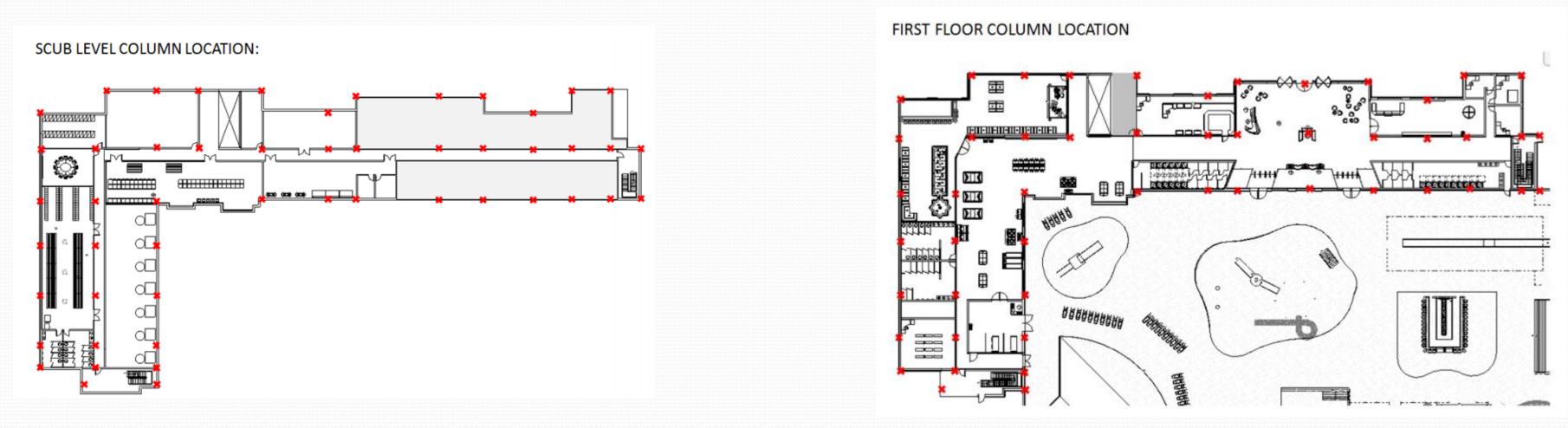
- Normal Weight Concrete
- No- Shoring Needed
- Spray on Fireproofing Required

Designed Decking: Vulcraft 1.5VLR 20







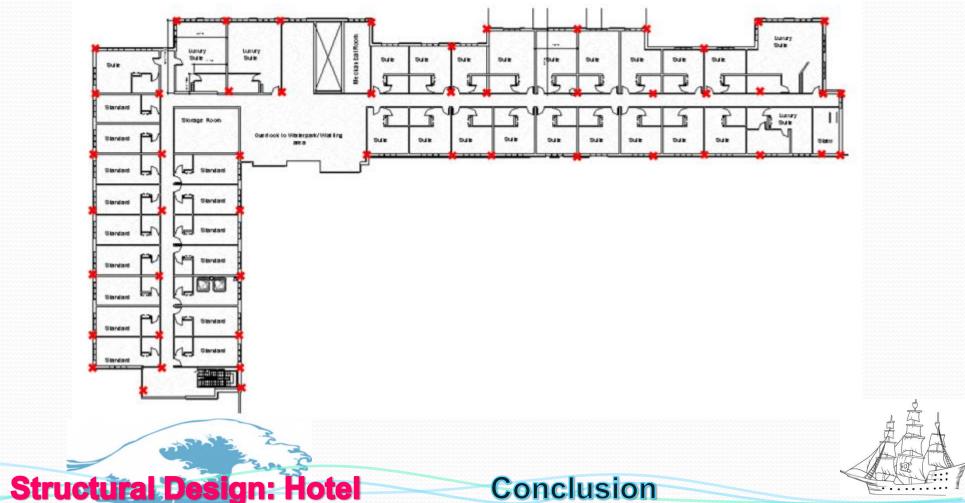


Architectural Design

Structural Design: Hotel Gravity System

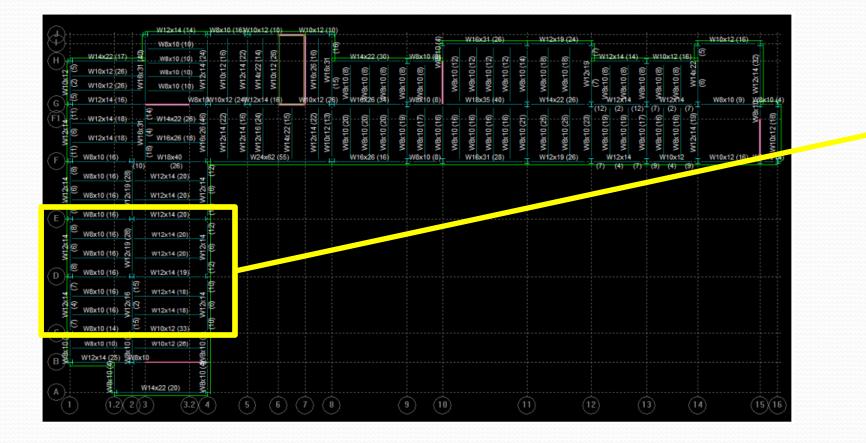
Structural Design Water Park

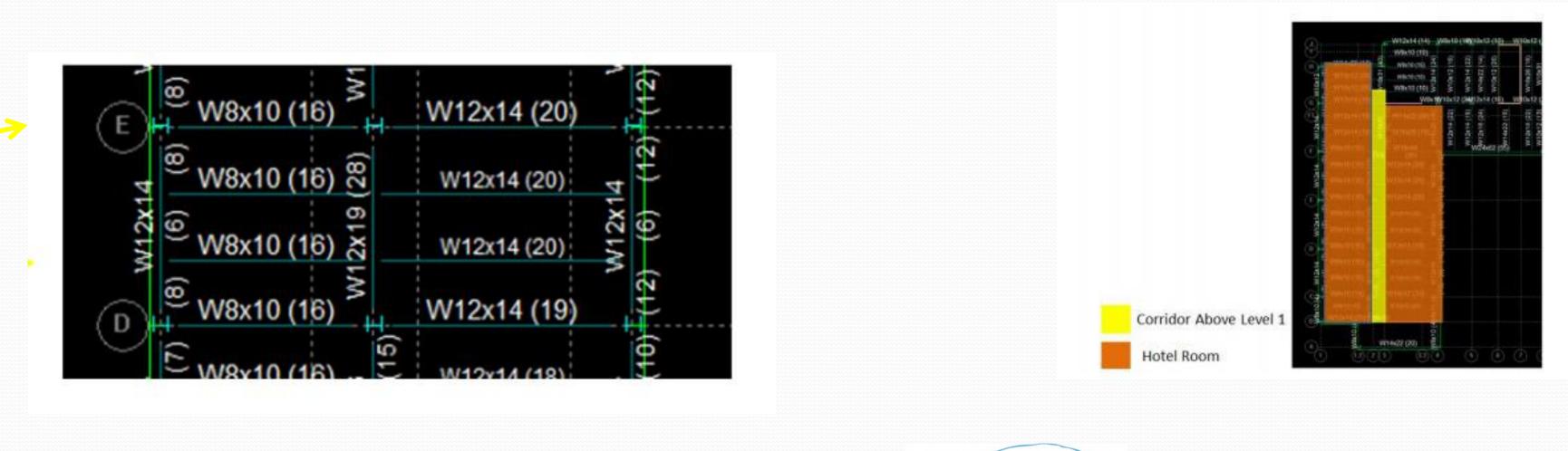
2-7TH FLOOR COLUMN LOCATION





Typical Bay Design (Floor 2-7)





Structural Design: Hotel

Problem Statement Introduction Blackbeard's



Structural Design: Hotel Gravity System



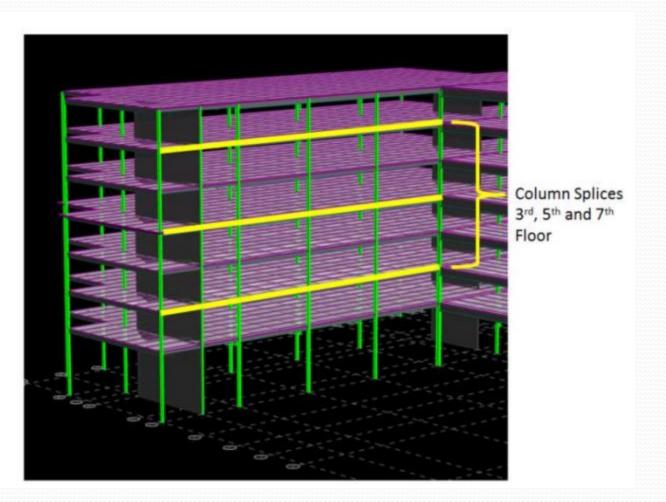
Structural Design Water Park

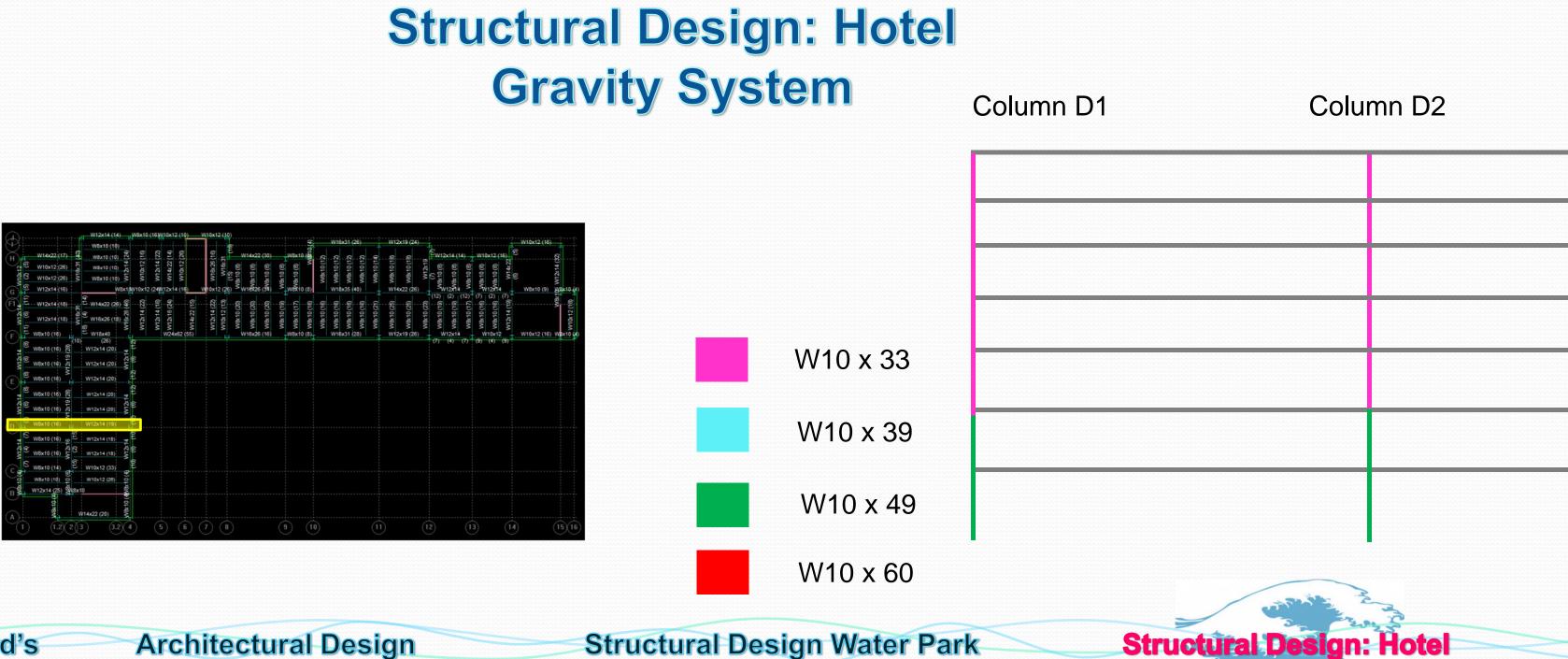
Typical Bay Loading





Column Splice Locations





Problem Statement Introduction Blackbeard's

Column D4

Conclusion	

Lateral System:

Shear Wall Information:

- 7 Ordinary Concrete Shear Walls 0 7
- o 12" Thick
- Similar Design to Prince Frederick Hall

Change to Original Shear Walls:

• Shear Wall #2 was moved- Architectural

Floor Plans

• Higher Loading Conditions: Updated Code

Introduction Blackbeard's **Problem Statement**



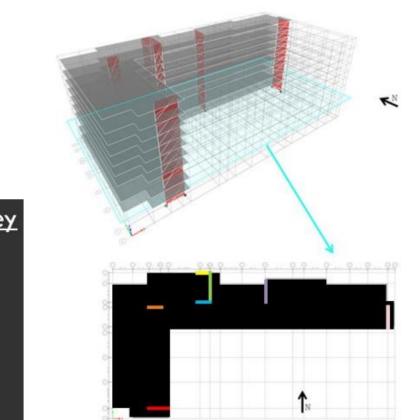


She



Architectural Design

Structural Design: Hotel Lateral System



Shear Wall Key

ar	Wall 2	
ar	Wall 3	
ar	Wall 4	
ar	Wall 5	
ar	Wall 6	
ar	Wall 7	

Structural Ram Model

Structural Design Water Park

Controlling Wind Load Deflections:

Case 3: Wind Loading 0.75 Y + Moment		
Level	Max Deflection (Inches)	
Roof	1.728964	
7th	1.483152	
6th	1.27641	
5th	1.071233	
4th	0.869805	
3rd	0.676528	
2nd	0.496462	
1st	0.224036	

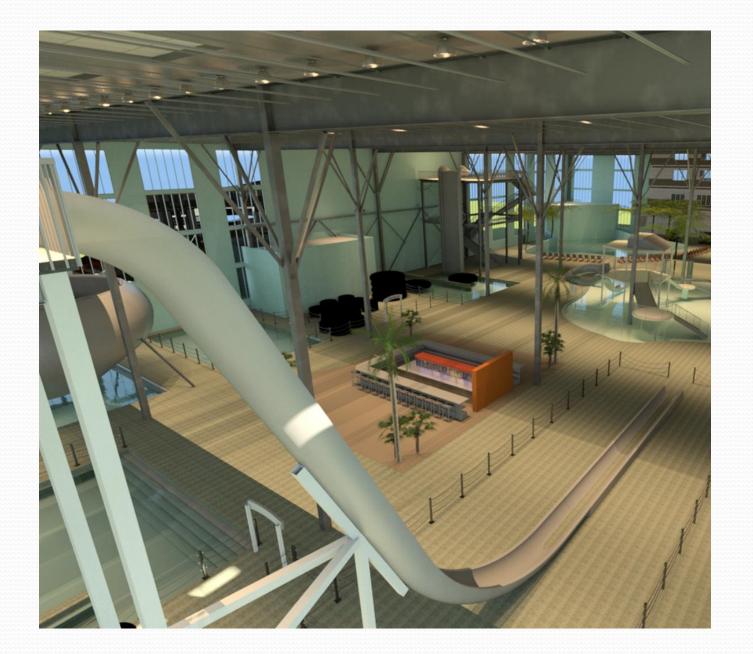
Seismic Loading Deflections:

Seismic Loading		
Level Max Deflection (Inches)		
Roof	1.031962	
7th	0.891212	
6th	0.773018	
5th	0.655653	
4th	0.540096	
3rd	0.427802	
2nd	0.320811	
1st	0.152055	



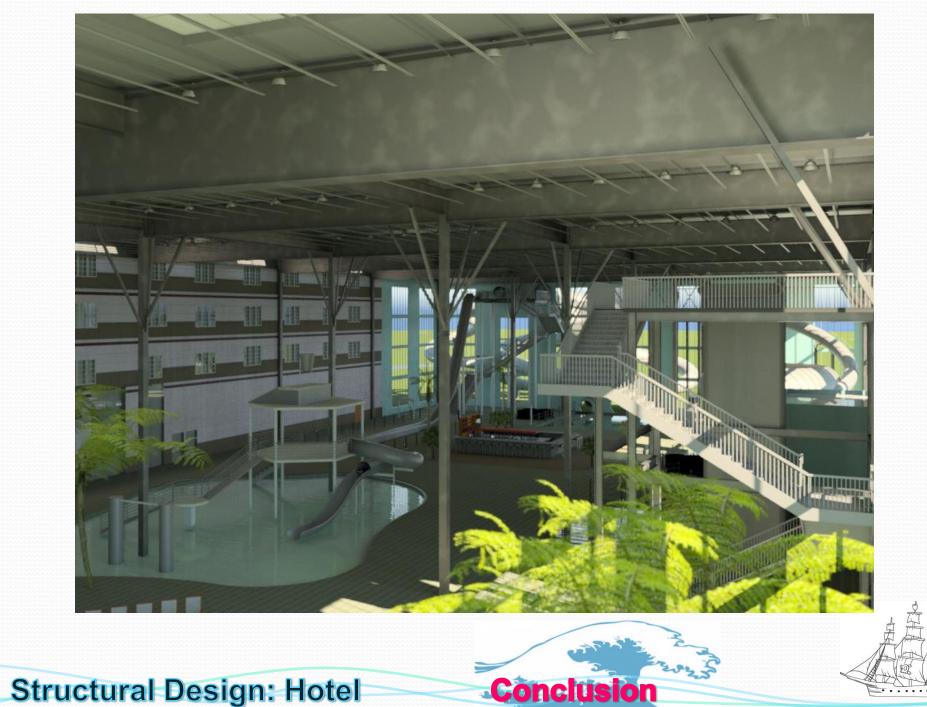




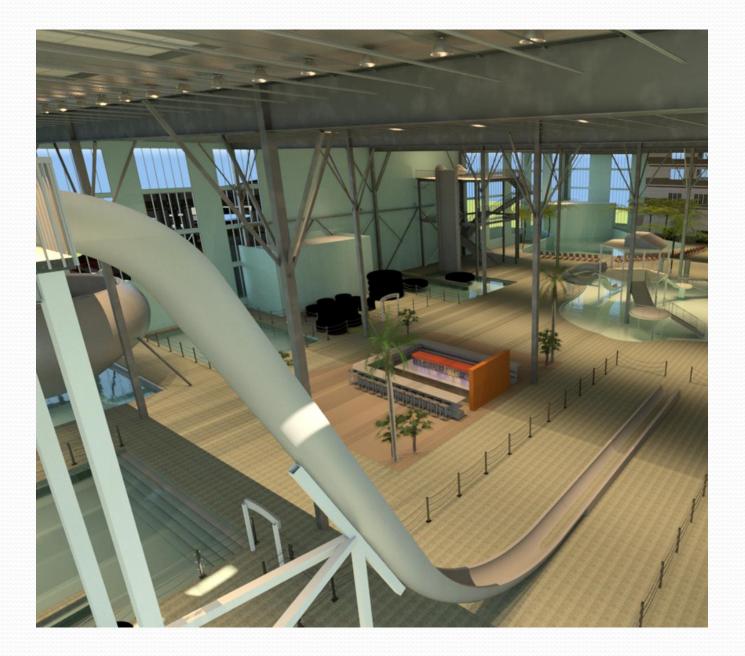




- A Exciting New Family Resort Was Created
- Architectural Design of Floor Plans Were Created
- Dynamic Loading Was Explored
- Water Slide Structure Was Designed
- Large Spanning Members were Designed For the Water Park
- Lateral Frames Were Designed
- Hotel Gravity and Lateral Were Explored







Problem Statement





Acknowledgements

Entire AE Faculty

Professor Heather Sustersic Dr. Thomas Boothby Dr. Linda Hanagan Professor Kevin Parfitt

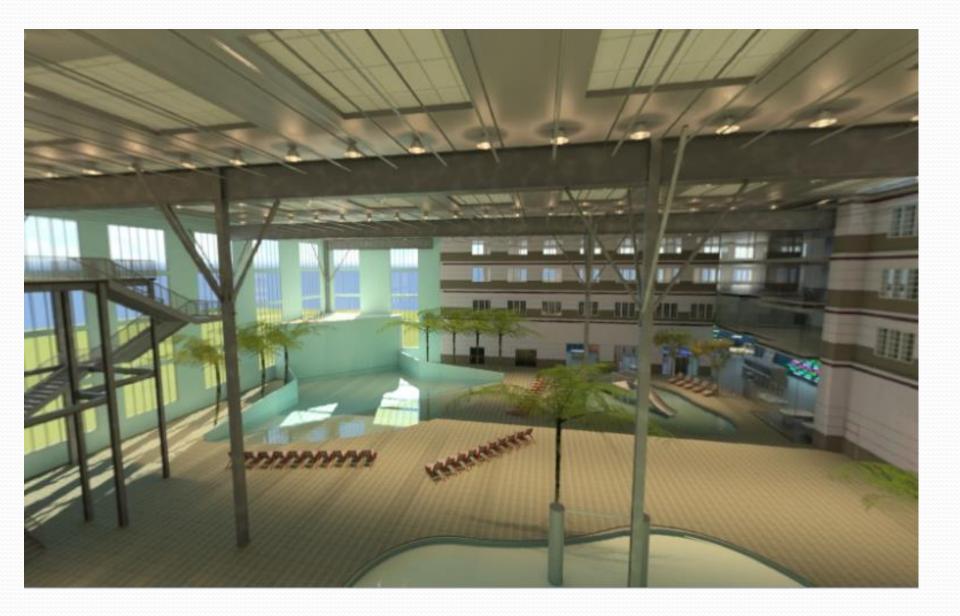
Fellow AE Friends

Friends and Family











QUESTIONS?

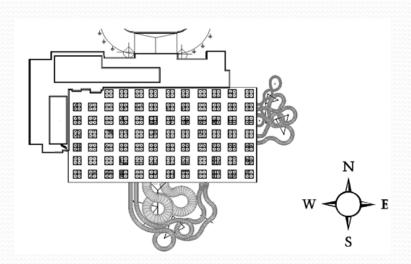






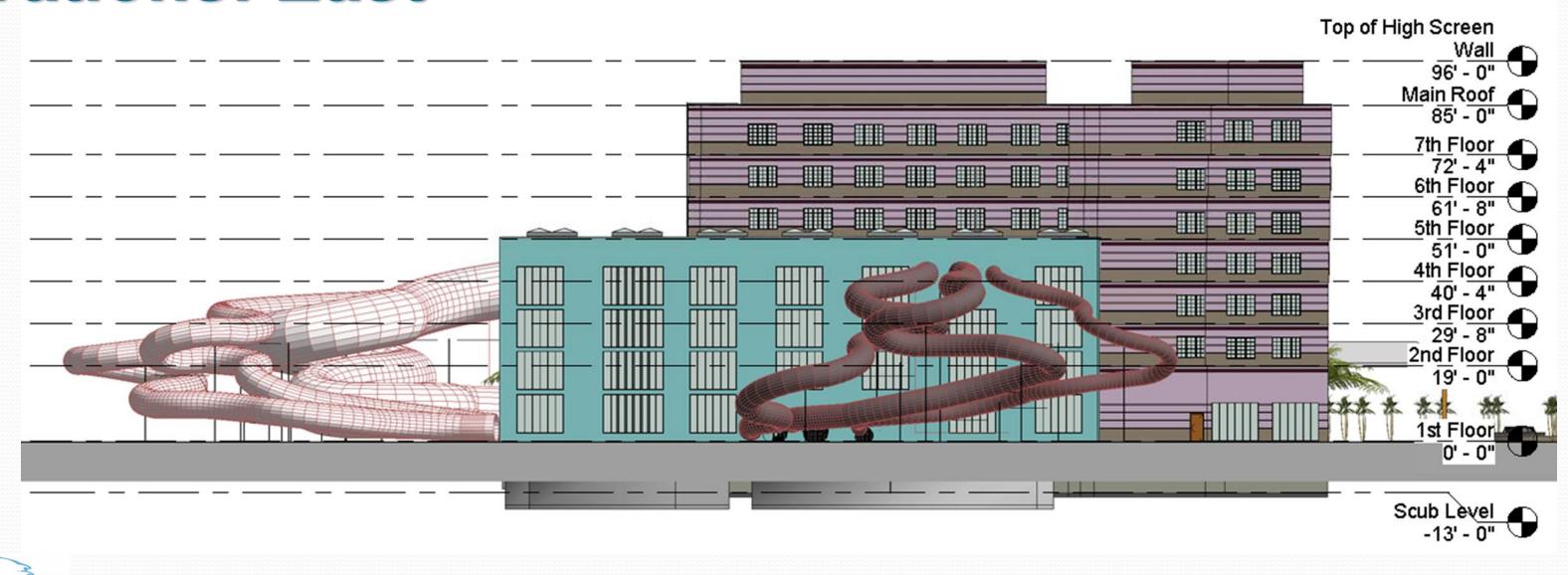
New Building Elevations: North



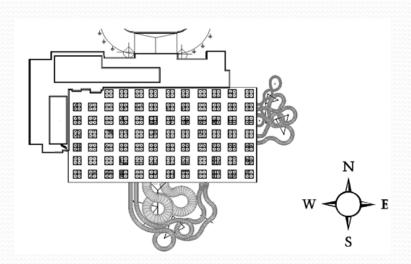




New Building Elevations: East









Economy Joist Table:

APPENDIX



LRFD

0K7	22K10	28K8	28K9	24K10	30K8	30K9	22K11	26K10	28K10	30K10	24K12	30K11	26K12	28K12	30K12
30	22	28	28	24	30	30	22	26	28	30	24	30	26	28	30
2.3	12.6	12.7	13	13.1	13.2	13.4	13.8	13.8	14.3	15	16	16.4	16.6	17.1	17.6
							1000								
	825 548						825 548								
	825 518						825 51ft								
	825			825			825				825				
	825			825			825 474				825				
-	825			825			825	825			825		825	-	-
-	454			499			454 825	541 825			400 825		541 825	-	
_	432	8.75	876	479	-	_	432	522	0.00	_	479	_	522	805	
	825 413	825 543	825 543	825 456		_	825 413	825	825 543		825 456		825 501	825 543	
	825 399	825 522	825	825 436			825 399	825 478	825 522		825 436		825 479	825 522	
825 543	825 385	825 500	825 500	825	825 543	825 543	825 385	825	825 500	825 543	825 422	825 543	825 459	825 500	825
801	825	825	825	825	825 520	825	825	825	825 480	825	825 410	825	825	825	825
751	775	772	823	823	823	823	823	823	823	823	823	823	823	823	823
461 706	337 729	438	463	393 798	500	500	355	431 798	463	500 798	393 798	798	431 798	463 798	500
420	307	399 584	432	368 753	460 735	468	334	404	435	468	368	468	404	435	458
384	280	364	295	337	420	441	314	378	410	441	344	441	378	410	441
827 351	648 257	645 333	702	709 306	693 384	751 415	741 292	751 356	751 389	751 415	751	751 415	751	751 389	751 415
582 323	612 236	609 306	663 332	670 283	654 353	712 383	700 269	729	730	730	730	730	730	730	730
559 297	579 217	576	627	634 260	619 325	673 352	663 247	890 306	711	711	711 290	711	711	711	711
531	549	546 260	594 282	601 240	586	639	628	654	691	691	601	691	691 299	691	691
504	520	519	564	570	556	606	595	619	670	673	673	673	673	673	673
478	185	240 492	535	222	529	300	211 565	262	306 636	333 657	261 657	657	283 657	306	333 657
234	471	222	241	206	256 502	278	105 538	243	284	315	247	315 640	269	291	315
433	158	206	224 486	191	238	258	181	225	263	300	235	300 625	258	277	300
202	148	192	208	177	221	240	168	210	245	282	224	284	244	264	284
414 188	427 138	426	463 194	468	457 206	498	489 157	508 195	550 228	591 263	609 213	610 270	610 232	610 252	610 270
394 176	408	408	442	447	436 192	475 208	466	486	525 212	564 245	580	597 258	587	597 240	597 258
376		388 158	423	427	417	454		465	501 198	538	555 185	583	583	583	583
361		372	405	408	399	435		444	480	516	531	570	570	570	570
345		355	387	135 391	168 382	182 415		426	459	214 493	508	236 558	203 553	219 558	236 558
144 331		136	148	126	157	171		149	174	201 472	163 487	226 543	192	210	226
135		128	138	118	148	160	2	140	163	188	153	215	180	201	216
127		120	130		139	150		131	153	177		1000	169	193	207
304 119		313 113	342		337 130	367		375	405	436		499	487 158	525 185	525 199
292	-	301	328	1	324	352		361	390 136	418	()	480	469	507	514



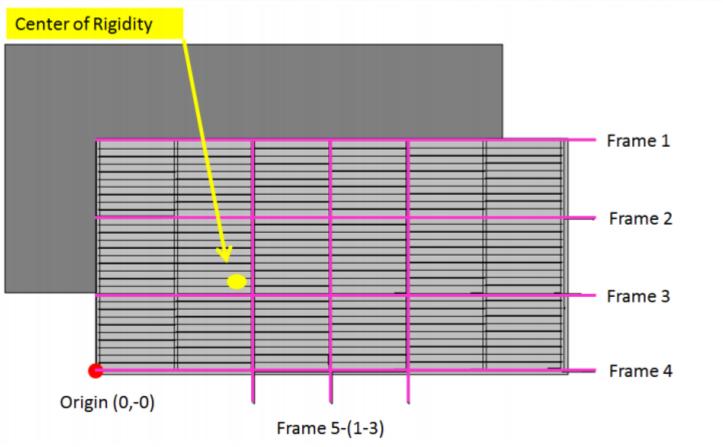
Water Park Frame Stiffness:

Deflection (inch) {Dummy Load}	Stiffness K (K/in)
0.039	25.60
0.021	47.60
0.024	41.67
0.021	47.60
0.007	142.80
	{Dummy Load} 0.039 0.021 0.024 0.021



Water Park Center of Rigidity :

Indoor Water Park Center of Rigidity									
	Distance From Zero Reference			Relative Rigidity					
Element	X (Ft)	Y (Ft)	Rx	Ry	RxY	RyX			
Frame 1	150	150	25.6	0	3840	0			
Frame 2	150	100	47.6	0	4760	0			
Frame 3	150	50	41.67	0	2083.5	0			
Frame 4	150	0	47.6	0	0	0			
Frame 5-1	75	100	0	142.8	0	10710			
Frame 5-2	75	150	0	142.8	0	10710			
Frame 5-3	75	200	0	142.8	0	10710			
								X bar r	Y bar r
Totals			162.47	428.4	10683.5	32130		75	65.75676





Water Park Wind Loading:

Wind Loading N
Height
5
10
15
20
25
30
35
40
45
50
51
Height
5
10
15
20
25
30
35
40
45
50
51



1	h-South Water	Park					
	Zg	α	Kz	Kzt	Kd	V	qz
	1200	7	0.57472	1	0.85	115	16.539
	1200	7	0.57472	1	0.85	115	16.539
	1200	7	0.57472	1	0.85	115	16.539
	1200	7	0.623954	1	0.85	115	17.955
	1200	7	0.66503	1	0.85	115	19.13
	1200	7	0.700591	1	0.85	115	20.161
	1200	7	0.732137	1	0.85	115	21.069
	1200	7	0.760609	1	0.85	115	21.888
	1200	7	0.786641	1	0.85	115	22.637
	1200	7	0.810681	1	0.85	115	23.329
	1200	7	0.815281	1	0.85	115	23.461
			_				
	qz	G	h/L	Ср	Срі	Р	
	16.53905277	1.2	0.34	0.8	0.18	12.900461	
	16.53905277	1.2	0.34	0.8	0.18	12.900461	
	16.53905277	1.2	0.34	0.8	0.18	12.900461	
	17.95590979	1.2	0.34	0.8	0.18	14.00561	
	19.13797531	1.2	0.34	0.8	0.18	14.927621	
	20.16133115	1.2	0.34	0.8	0.18	15.725838	R
	21.06914234	1.2	0.34	0.8	0.18	16.433931	0
	21.8884992	1.2	0.34	0.8	0.18	17.073029	
	22.63763177	1.2	0.34	0.8	0.18	17.657353	h
	23.32945321	1.2	0.34	0.8	0.18	18.196974	h
	23.46182289	1.2	0.34	0.8	0.18	18.300222	>

Roof Pressure								
0-h/2	0-25.5	0.9	16.47					
h/2-h	25.5-51	0.9	16.47					
h-2h	51-102	0.5	9.15					
>2h	102-150	0.3	5.49					

						000
Vind Loading Ea	st to West					
Height	Zg	α	Kz	Kzt	Kd	
5	1200	7	0.57472	1	0.85	
10	1200	7	0.57472	1	0.85	
15	1200	7	0.57472	1	0.85	
20	1200	7	0.623954	1	0.85	
25	1200	7	0.66503	1	0.85	
30	1200	7	0.700591	1	0.85	
35	1200	7	0.732137	1	0.85	
40	1200	7	0.760609	1	0.85	
45	1200	7	0.786641	1	0.85	
50	1200	7	0.810681	1	0.85	
51	1200	7	0.815281	1	0.85	
Height	qz	G	h/L	Ср	Срі	
5	16.53905277	1	0.34	0.8	0.18	1
10	16.53905277	1	0.34	0.8	0.18	1
15	16.53905277	1	0.34	0.8	0.18	1
20	17.95590979	1	0.34	0.8	0.18	1

Height	qz	G	h/L	Ср	Срі	Р
5	16.53905277	1	0.34	0.8	0.18	10.254213
10	16.53905277	1	0.34	0.8	0.18	10.254213
15	16.53905277	1	0.34	0.8	0.18	10.254213
20	17.95590979	1	0.34	0.8	0.18	11.132664
25	19.13797531	1	0.34	0.8	0.18	11.865545
30	20.16133115	1	0.34	0.8	0.18	12.500025
35	21.06914234	1	0.34	0.8	0.18	13.062868
40	21.8884992	1	0.34	0.8	0.18	13.57087
45	22.63763177	1	0.34	0.8	0.18	14.035332
50	23.32945321	1	0.34	0.8	0.18	14.464261
51	23.46182289	1	0.34	0.8	0.18	14.54633

V	qz
115	16.5391
115	16.5391
115	16.5391
115	17.9559
115	19.138
115	20.1613
115	21.0691
115	21.8885
115	22.6376
115	23.3295
115	23.4618

Roof Pressure								
0-h/2	0-25.5	0.9	13.05					
h/2-h	25.5-51	0.9	13.05					
h-2h	51-102	0.5	7.25					
>2h	102-300	0.3	4.35					



Water Park Seismic	l aadima.							_	
VULUEI FAIM OGIDIIIU	LOQUIIGO	Indoor Water Park W	Veight						
		Members	Quantity	Weight (lbs/ft)	Length (ft)	Total Weight (Kips)			
		Joists	162	16.4	50	132.84			
		Member	Quantity	Weight (lbs/cft)	Area(ft)	Length(ft)	Total Weight(Kips)		
		Plate Girder 1	19	0.28			1.40315	j	
		Plate Girder 2	1	0.28			1.2264	ļ	
		Plate Girder 3	24	0.28	19.75	50	6.636	; 	<u> </u>
		Member	length(ft)	Width(ft)	Area	Weight (psf)	Total Weight		
		Built-up Roof	300	150			900)	
		Hvac	300	150	4500) 12	54	Ļ	
							Total Weight Roof (kips)		
							1096.10555		
		Column Size	Quantity	Length(ft)	Weight(plf)	Total Weight (kips)			
		HSS 14 x 14 x 5/8	23	51	110	129.03			
		HSS 12 x 12 x 5/8	3	51	93.34	14.28102			
		W 14 x 257	2	51	257	26.214			
		HSS 3.5 x 3.5 x 5/8	94	20	14.72	27.6736			
							Total Weight (kips)		
							197.19862	2	
		Seismic Loading Wat	ter Park						
				R	Ω	Cd			
		Steel Eccentrically E	Braced Frames	8	3	5.5			
		Seismic Base Shear							
		Fa	Ss	Sms	Sds	lc	Cs	w	V
		1	0.75	0.75	0.5	1	0.0625	1293.304	80.83151
					<u> </u>				
APPENDIX					~				\leq



Hotel Structure Floor Plans: First Floor

W12x14 (14)W8x10	0 (16)W(10x12 (10) W10x12 (10)			
W8x10(10)	····			W12x16 (28)
H) W14x22(17) 8	(2 (4 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2		ຊ. <u>ຄ</u>	8,10 (20) (10) (
H W14x22'(17) W10x12'(26)	W12x14 (22) W14x22 (14) W10x12 (26) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W16x31 (15) W17x14 (22) W16x31 (15) W16x311 W16x31 W16x31 W16x31 W16x31 W16x311 W16x	8x10 (8) 8x10 (8) 1 1 1 1 1 1 1 1 1 1 1 1 1	W8x10(12) W8x10(14) W8x10(14) W8x10(14) W8x10(15) W12x19 W12x19 W12x19 W12x19 W12x19	(10) (10) (10) (10) (10) (10) (10) (10)
		88) 01 03 01 01 03 01 01 03 01 05 01 05 00 00 00 00 00 00 00 00 00	(40) W14x22 (26) W14x22 (26)	
W12x14 (16) W8x10/V10x1			$= \frac{W_{14x22}(26)}{(12)} + \frac{W_{12x14}}{(12)} + \frac$	(12) + (7) + (2) + (7)
F1 +	1 (16) 3 (24) 2 (15) 2 (13) 2	(19) (19) (19) (19) (19) (19) (19) (19)	(16) (25) (25) (25) (25) (19) (19) (19)	(13) (12) (13) (14) (14) (15) (12) (12) (12) (12) (12) (12) (12) (12
F1 E	W12x14 (16) W12x16 (24) W14x22 (15) W12x14 (22) W10x12 (13) W8x10 (20) W8x10 (20)	W8x10 (20) W8x10 (19) W8x10 (17) W8x10 (16) W8x10 (16) W8x10 (16)	W8x10 (16) W8x10 (21) W8x10 (25) W8x10 (25) W8x10 (23) W8x10 (19)	W8x10(17) W8x10(16) W8x10(16) W8x10(12) W8x10(12) W8x10(12) W8x10(12) W8x10(12)
(F) ₩8x10 (16) ₩18x40 ≥ ≥	W12x16 (15) W12x16 (24) W12x16 (24) W12x14 (22) W12x14 (22) W12x14 (22) W12x14 (22) W12x14 (22) W12x14 (22) W12x14 (22)	≤ ≤ ≤ ≤ ≤ ≤ 26 (16)W8x10 (8)W16x31		
			(7) (4)	(7) + (9) (4) (9) + + + + + + + + + + + + + + + + + + +

W8x10 (16) W12x14 (20)				
(E) W8x10 (16) H W12x14 (20)				
4 100010 (10) 1 112014 (20); 4				
W8x10 (10) C W12x14 (20) F W8x10 (10) 6L XL W12x14 (20) F W8x10 (10) KL W12x14 (20) KL KL				
(D) ₩8x10 (16) ₩ W12x14 (19)				
0 X14 (0) 11 X14				
W8x10 (10) W10x12 (26) W10x12 (26) W10x1				
B W12x14 (25) W8x10				
W8x10 (10) W10x12 (28) P W12x14 (25) W10x12 (28) P				
$\begin{array}{c} (A) \\ (1) \\ (1.2) \\ (2) \\ (3) \\ (3.2) \\ (4) \\ (4) \\ (1) \\ ($	(5) (6) (7) (8)	(9) (10)	(11) (12)	(13) (14) (15)(16)





Hotel Structure Floor Plans: 2nd -7th

	W10x12(10)		
(P)	€	W12x19 (24)	W12x16 (28)
H W14x22'(17) G W8x10 (10) (10) (10) (10) (10) (10) (10) (1		(1) 01 00 00	W12×16 W8×10 (10) W8×10 (10) W8×10 (10) W10×12 (30)
	(40) (31) (31) (40)	(E) 01 W W W 10 (C)	∑ (000 000 000 000 000 000 000 000 000 0
		1 (12) (2) (12) (12) (7) (2) (7 (7) (2) (7 (7) (2) (7 (7) (2) (7 (7) (2) (7) (2) (7 (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (2) (7) (7) (7) (7) (7) (7) (7) (7) (7) (7	
00 W12x14 (18) W16x26 (19) 92 W12x14 (18) W16x26 (19) W12x14 (18) W16x26 (19)	W12x14 (22) W12x12 (13) W8x10 (20) W8x10 (20) W8x10 (19) W8x10 (16) W8x10 (16) W8x10 (16) W8x10 (16) W8x10 (16)	W8x10(2) W8x10(2) W8x10(2) W8x10(2) W8x10(2) W8x10(1) W8x10(2) W8x10(1) W8x	H M8x10(12) W8x10(12) W8x10(12) W8x10(12) W8x10(12) W8x10(12) W8x10(12) W8x10(12) W8x10(12)
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	S S	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	W12x19 (20) W4x10 (4)
W8x10 (16) 👸 W12x14 (20) 🚽			
χ (C) W8x10 (16) χ W12x14 (20) Σ (C)			
D ₩8x10 (16) W12x14 (19)			
(f) (g) (g) <td></td> <td></td> <td></td>			
E W8y10 (14) E W10y12 (33) E			
A W14x22 (20)			
$ \begin{array}{c} (1) \\ (1.2)(2)(3) \\ (3.2)(4) \\ (5) \\ (6) \\ (6) \\ (1)(1-1)(1-1)(1-1)(1-1)(1-1)(1-1)(1-1)($	7 (8) (9) (10) (1	11) (12) (13)	(14) (15)(16)





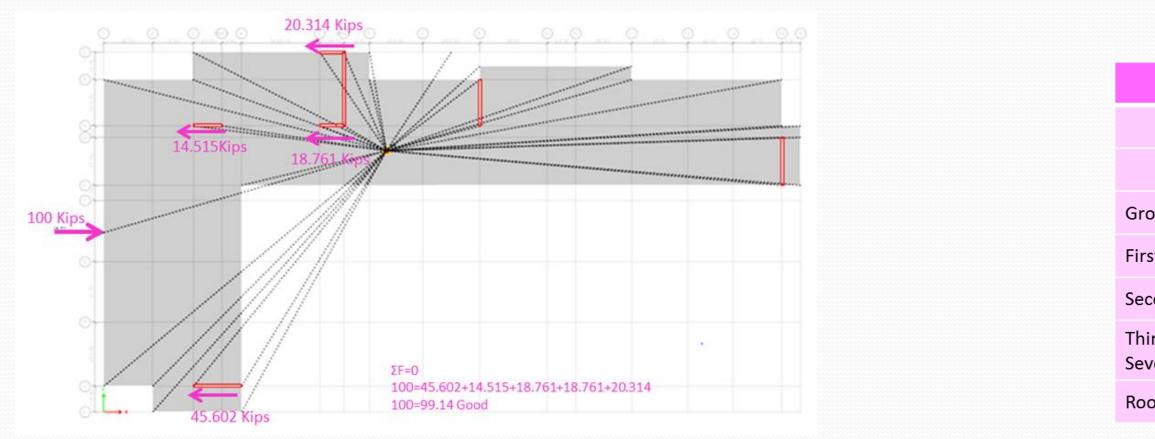
Hotel Structure Floor Plans: Roof

A		W12x16 (30) W	/14x22 (12 <mark>)//</mark> 12x14 (10)	<mark>W10x12 (10</mark>)	J		L
$\langle \mathcal{P} \rangle$				ெ	€W14x2		W10x12 (24)
н	W12x16 (34) है		(54) (28) (28)	W16x26 (16) W16x26 (16) W16x26 (16) W10 (8) (16) W10 (8) (16) W10 (8) (16) W10 (8) (16) W10 (8) (16) W10 (8) (16) W10 (1		କକକକ _N	x12 (8) W8x10 (12)
9	W8x10 (11) *	W14x22 (16) X W14x22 (16) X W14x22 (16) X	W16x26 (54) W16x26 (36) W16x26 (24) W12x19 (28)	M16x26 (11 W16x26 (1) (9) ×10 (8) ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) 15 ×10 (8) ×10 ×10 ×10 ×10 ×10 ×10 ×10 ×10 ×10 ×10	8x10 (8) H 8x10 (8) w(8x10 (9) w(8x10 (9) w(9x10 (9) w(9x10 (9) w(9x10 (9) (9) w(9x10 (9) (9) (9) (9) (9) (9) (9) (9) (9) (9)	wex10(9) W8x10(9) W8x10(9) W8x10(9) W8x10(9) W8x10(9) M10x12	8x10 (8) 8x10 (8) 8x10 (8) 0 0 0 0 0 0 0 0 0 0 0 0 0
8x10	W8x10 (11)	W14x22 (16) 🕺	W1 W1 W1	(0) (0) (0) (0) (0) (0) (0) (0) (0) (0)		W8 W8 W8	x15 (9) W8x10 (15) W8x10 (9) W8x10 (12) W8x10 (13) W8x10
D WBx10(6)	W8x10 (11)	W8×104	/16x26 (2000/14x22 (14)	W12x14 (24) SW18x35 (70)	^S w10x12 (12) W21x4	4 (60) W8x10 (9) SW	8x70 ⁵ ⁵ W8x70 W8x10 W8x10 (4)
W10x12(10)	W8x10 (11) - 🤤	W16x26 (16)	¹ 33 ¹ 38 ¹ 4	20 16 16	6 6 6 6 6	<u>4</u> <u>4</u> <u>6</u> <u>6</u> <u>6</u> <u>6</u> <u>6</u>	(2) (3) + (3) (2) (3) + (2) (2) (2) (2) (2) - • • • • • • • • • • • • • • • • • • •
×12(22 (W16x26 (18)	W14x22 (20) W14x22 (20) W16x26 (18) 66x 66x 60x 60x 99 W16x26 (22)	W14x22 (20) W12x19 (24) W14x22 (16) W14x22 (16) Fpt tr W14x22 (16) W14x22 (16)	W14x22 (16) W14x22 (14) W14x22 (14) W14x22 (14) W14x22 (14)	W14x22 (14) W14x22 (14) W10x12 (16) W8x10 (8) W8x10 (8) W8x10 (8)	W8x10 (8) W8x10 (8) W8x10 (8) W8x10 (8) W8x10 (8) W8x10 (8) W8x10 (8) W8x10 (2)
W10	W8x10 (11) 🐳	W16x26 (18)	W14	W14; W12; W14; W14;	W14) W14) W14) W14)	W14	W8 W8 W8 W8 W8 W8 W8
(F)#	W8x10 (9)	W18x40 (60)	W30x99 (56)	W21x44 (36)	W12x14 (16) W242 (6) (6) (2)		$x_{12}(8)$ $+$ W8x10 (12) $+$ W10x12 (24) W8x10 (4)
(12)	W8x10 (9) 🖉	W18x35 (30)			(0) (0) (2) (6) (6) + +	
k12	W8x10 (9) K	W18x35 (30)	Ê				
W10x12 (12)	6)	>					
(E)	W8x10 (9)	TTTORES (SO)					
(12)	W8x10 (9) g	W18x35 (30) မ္က					
W10x12(12)	W8x10 (9)	W18x35 (30)	Đ				
W1	(9)						
	W8x10 (9)	1110201 (00)					
(10)	W8x10 (9) (9)	W16x31 (64) 6	2				
0x12	W8x10 (9) 5 00	W16x31 (64)					
W1	W8x10 (9)	W16x26 (66)	2				
00000000000000000000000000000000000000		000					
VBX1	W8x10 (9) W12x14 (13) W8x10	W16x26 (44) 7 X					
	<u> </u>	(
0	N8x10	16x26 (26)					
(A)) (1.2) 2) 3	<u> </u>) (5) (6) (7) (8)	(9) (10)	(11) (12)	(13) (14) (15)(16)
Ċ						\odot	





ETABS Model Check and COR:





Center of Rigidity: Hand Calculations vs. ETABS

	Hand Cal	culations	ETABS Calculation					
	Х	Y	Х	Y				
round Floor	168.4	81.0	164.8	73.2				
rst Floor	175.5	88.0	150.0	70.0				
cond Floor	168.4	81.0	138.7	68.0				
nird to eventh Floor	177.5	112.2	120.0	70.0				
oof	175.8	88.4	130.0	70.0				



Hotel Wind Loading:

Wind Loadi	ng Hotel E	ast-West															
Height (ft)	B (ft)	L (ft)	V (mph)	Kd	Kzt	G	Gcpi	Zg	Kz	Q	Ср	Pww	Plw	Pt	Trib Width	Trib Height	F
15	160	320	115	0.85	1	0.85	0.18	0.85	0.623954	17.95591	. 0.8	8.977955	15.2586	24.23655	160	9.5	36.839
19	160	320	115	0.85	1	0.85	0.18	0.9	0.667552	19.21054	0.8	9.605269	15.2586	24.86387	160	7.3	29.0
30	160	320	115	0.85	1	0.85	0.18	0.98	0.760609	21.8885	0.8	10.94425	15.2586	26.20285	160	10.6	44.440
40	160	320	115	0.85	1	0.85	0.18	1.04	0.825768	23.76363	0.8	11.88181	15.2586	27.14041	160	10.6	46.030
51	160	320	115	0.85	1	0.85	0.18	1.09	0.885124	25.47174	0.8	12.73587	15.2586	27.99447	160	10.6	47.478
62	160	320	115	0.85	1	0.85	0.18	1.13	0.93592	26.93353	0.8	13.46676	15.2586	28.72536	160	10.6	48.718
72	160	320	115	0.85	1	0.85	0.18	1.17	0.976772	28.10915	0.8	14.05458	15.2586	29.31318	160	10.6	49.715
85	160	320	115	0.85	1	0.85	0.18	1.24	1.024211	29.47433	0.8	14.73716	15.2586	29.99576	160	10.8	51.832
96	160	320	115	0.85	1	0.85	0.18	1.26	1.060449	30.51719	0.8	15.2586	15.2586	30.5172	160	5.5	26.8551
المحمل المحمل	n a llatal N		h.														
Wind Loadi				Kd	Kzt	G	Coni	7.0	Kz	P	0	Dunu	Plw	Pt	Tails Wisteh	Trib Height	F
Height (ft)		L(ft)				-	Gcpi	Zg		•	-	Pww				~	•
15	320	160	115	0.85		0.85											
19	320	160	115	0.85	1	0.85	0.18	0.9	0.614877	17.69468	3 0.8	8.84734	14.05458	22.90192	360	7.3	60.186
30	320	160	115	0.85	1	0.85	0.18	0.98	0.700591	20.16133	0.8	10.08067	14.05458	24.13525	360	10.6	92.10
40	320	160	115	0.85	1	0.85	0.18	1.04	0.760609	21.8885	0.8	10.94425	14.05458	24.99883	360	10.6	95.395
51	320	160	115	0.85	1	0.85	0.18	1.09	0.815281	23.46182	0.8	11.73091	14.05458	25.78549	360	10.6	98.397
	320	100			-	0.05	0.18	1.13	0.862069	24.80827	0.8	12.40413	14.05458	26.45871	360	10.0	100.96
62	520	160	115	0.85	1	0.85	0.10	1,13	0.002003	24.00027	0.0	12.40415	14.00400	20.450/1	200	10.6	100.90
62 72	320	160	115 115	0.85		0.85				25.89113							0.
<u> </u>					1	<u></u>	0.18	1.17		25.89113	0.8	12.94556	14.05458	27.00014	360	10.6	103.03

Wind Loadi	ng Hotel E	ast-West															
Height (ft)	B (ft)	L (ft)	V (mph)	Kd	Kzt	G	Gcpi	Zg	Kz	Q	Ср	Pww	Plw	Pt	Trib Width	Trib Height	F
15	160	320	115	0.85	1	0.85	0.18	0.85	0.623954	17.95591	0.8	8.977955	15.2586	24.23655	160	9.5	36.83956
19	160	320	115	0.85	1	0.85	0.18	0.9	0.667552	19.21054	0.8	9.605269	15.2586	24.86387	160	7.3	29.041
30	160	320	115	0.85	1	0.85	0.18	0.98	0.760609	21.8885	0.8	10.94425	15.2586	26.20285	160	10.6	44.44003
40	160	320	115	0.85	1	0.85	0.18	1.04	0.825768	23.76363	0.8	11.88181	15.2586	27.14041	160	10.6	46.03014
51	160	320	115	0.85	1	0.85	0.18	1.09	0.885124	25.47174	0.8	12.73587	15.2586	27.99447	160	10.6	47.47862
62	160	320	115	0.85	1	0.85	0.18	1.13	0.93592	26.93353	0.8	13.46676	15.2586	28.72536	160	10.6	48.71822
72	160	320	115	0.85	1	0.85	0.18	1.17	0.976772	28.10915	0.8	14.05458	15.2586	29.31318	160	10.6	49.71515
85	160	320	115	0.85	1	0.85	0.18	1.24	1.024211	29.47433	0.8	14.73716	15.2586	29.99576	160	10.8	51.83268
96	160	320	115	0.85	1	0.85	0.18	1.26	1.060449	30.51719	0.8	15.2586	15.2586	30.5172	160	5.5	26.85513
Wind Loadi	ng Hotel N	orth-Sout	h											*****			
Height (ft)																	
	B(III)	L(ft)		Kd	Kzt	G	Gcpi	Zg	Kz	Р	Q	Pww	Plw	Pt	Trib Width	Trib Height	F
15	320	L (ft) 160		Kd 0.85	Kzt	G 0.85		Zg 0.85		P 16.53905		Pww 8.269526					· · · · · · · · · · · · · · · · · · ·
			V (mph)		Kzt 1 1		0.18	0.85	0.57472		0.8		14.05458	22.32411	360	9.5	76.34844
15	320	160	V (mph) 115	0.85	1 1	0.85	0.18 0.18	0.85	0.57472 0.614877	16.53905	0.8 0.8	8.269526 8.84734	14.05458 14.05458	22.32411 22.90192	360 360	9.5 7.3	76.34844 60.18625
15 19	320 320	160 160	V (mph) 115 115	0.85 0.85	1 1 1	0.85	0.18 0.18 0.18	0.85 0.9 0.98	0.57472 0.614877 0.700591	16.53905 17.69468	0.8 0.8 0.8	8.269526 8.84734	14.05458 14.05458 14.05458	22.32411 22.90192 24.13525	360 360 360	9.5 7.3 10.6	76.34844 60.18625 92.1001
15 19 30	320 320 320	160 160 160	V (mph) 115 115 115	0.85 0.85 0.85	1 1 1	0.85 0.85 0.85	0.18 0.18 0.18 0.18	0.85 0.9 0.98 1.04	0.57472 0.614877 0.700591 0.760609	16.53905 17.69468 20.16133	0.8 0.8 0.8 0.8	8.269526 8.84734 10.08067 10.94425	14.05458 14.05458 14.05458	22.32411 22.90192 24.13525 24.99883	360 360 360 360	9.5 7.3 10.6 10.6	76.34844 60.18625 92.1001 95.39553
15 19 30 40	320 320 320 320 320	160 160 160 160	V (mph) 115 115 115 115 115	0.85 0.85 0.85 0.85	1 1 1 1 1	0.85 0.85 0.85 0.85	0.18 0.18 0.18 0.18 0.18 0.18	0.85 0.9 0.98 1.04 1.09	0.57472 0.614877 0.700591 0.760609 0.815281	16.53905 17.69468 20.16133 21.8885 23.46182	0.8 0.8 0.8 0.8 0.8	8.269526 8.84734 10.08067 10.94425 11.73091	14.05458 14.05458 14.05458 14.05458 14.05458	22.32411 22.90192 24.13525 24.99883 25.78549	360 360 360 360 360	9.5 7.3 10.6 10.6 10.6	76.34844 60.18625 92.1001 95.39553 98.39744
15 19 30 40 51	320 320 320 320 320 320	160 160 160 160 160	V (mph) 115 115 115 115 115 115	0.85 0.85 0.85 0.85 0.85	1 1 1 1 1	0.85 0.85 0.85 0.85 0.85	0.18 0.18 0.18 0.18 0.18 0.18 0.18	0.85 0.9 1.04 1.09 1.13	0.57472 0.614877 0.700591 0.760609 0.815281	16.53905 17.69468 20.16133 21.8885 23.46182	0.8 0.8 0.8 0.8 0.8 0.8 0.8	8.269526 8.84734 10.08067 10.94425 11.73091 12.40413	14.05458 14.05458 14.05458 14.05458 14.05458 14.05458	22.32411 22.90192 24.13525 24.99883 25.78549 26.45871	360 360 360 360 360 360	9.5 7.3 10.6 10.6 10.6 10.6	76.34844 60.18625 92.1001 95.39553 98.39744 100.9665
15 19 30 40 51 62	320 320 320 320 320 320 320	160 160 160 160 160 160	V (mph) 115 115 115 115 115 115 115	0.85 0.85 0.85 0.85 0.85 0.85	1 1 1 1 1 1 1 1	0.85 0.85 0.85 0.85 0.85 0.85	0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18	0.85 0.9 0.98 1.04 1.09 1.13 1.17	0.57472 0.614877 0.700591 0.760609 0.815281 0.862069 0.899697	16.53905 17.69468 20.16133 21.8885 23.46182 24.80827	0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	8.269526 8.84734 10.08067 10.94425 11.73091 12.40413 12.94556	14.05458 14.05458 14.05458 14.05458 14.05458 14.05458 14.05458	22.32411 22.90192 24.13525 24.99883 25.78549 26.45871 27.00014	360 360 360 360 360 360 360	9.5 7.3 10.6 10.6 10.6 10.6 10.6	76.34844 60.18625 92.1001 95.39553 98.39744 100.9665 103.0326





APPENDI

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Primary U • Refer to p data shee specific ut information

S-W Pr

Epoxy Coating Comparison Chart

	Amine Epoxies	Polyamide Epoxies	Amidoamine Epoxies	Epoxy Phenolics/Novolacs				
Form very hard, achieve liters with escellent other and corrosion resistance Amine cured eponies an other used as protective costings and linings in highly corrosive environ- ments. Amine eponies require care in handling since the amines can be moderately initiating to takin, and may cause allergic reactions.		Polyamide epoxies generally offer the widest latitude in coating formulation. They are considered more realient and flexible, and have better weathering resistance and a longer pot life than amine cured epoxies. Polyamide epoxies generally have less solvent and acid resistance than amine cured epoxies.	Amidoamines are reaction products of a polyamine and a fatty acid. Their properties generally fail between those of amines and polyamides. They have good water and corrosion resistance like amines, and good toughness like polyamides. They have relatively small molecular size giving them low visc- ceties and making them very good surface wetters.	These coatings allow wild range formulating latitude Novolac epoxy resin increases chemical resistance and solvent resistance. Increasing the level of phenolic increases the chemical and solvent resistance, but the coating loses flexibility. Some phenolics require heat curing.				
ages	Excellent alkali and water resistance Very good add resistance Excellent solvent resistance Hard, abrasion resistant tilm Excellent corrosion resistance Excellent wetting of substate Chemical/moisture barrier	Very good alkali and water resistance Good add resistance Longer pot life than amines Easy to apply Cures more quickly than amines Good weathering characteristics Good film flexibility Excellent adhesion	Excellent surface wetting Excellent achesion Excellent water resistance Low viscosity Longer pot life than amines Good gloss retention	High heat resistance Excellent chemical resistance Excellent solvent resistance Excellent corrosion resistance Hard, abrasion resistant film				
antages/ ions	Amines can be initiating/toxic Relatively short recoat time Relatively short pot life Slover dry than normal polyamides Chalka/may discolor	Faster dry than amines Chalks High viscosity Temperature dependent Slow cure	Slow cure Fair color retention Temperature dependent	Some may require heat cure Relatively slow air cure Chalks/may discolor Relatively brittle				
y Uses o product neets for c use ation	Severe chemical resistant coating Barrier coating Othhore structures Storage tarks, structural steel Bridges, power plants Tarik linings Secondary containment	Water immersion General industrial Ottshore structures Storage tanks, structural steel Water/wastewater plants Tank linings Bridges, power plants Secondary containment	Barrier coating Surface tolerant coating Where chemical and moisture resistance is required General inclustrial Refinences Bindges, power plants	Severe chemical resistance Tark linings Secondary containment General Industrial Refineries Bridges, power plants				
oducts	Amines Shekote II Epoxy Shekote II Raka Filied Dura-Plate UHS Tank Clad HS Epoxy Sher-Glass FF Keltimines Dura-Plate MT Macropoxy 920 PhtPhme Phenalkamines Dura-Plate 235 Water-Based Vister-Based Vister-Based Vister-Based Vister-Based Find Clad DTM Visterbased Epoxy	Kern Catl-Coat HS Filer/Sealer Tile-Clad-High Solids Recoatable Epoxy Primer Copoxy Shop Primer Zinc Clad IV Zinc Clad III HS H4-Solids Catalyzed Epoxy Macropoxy 646 Faat Cure Macropoxy 646 Winter Grade Epolon II Primer Epolon II Primer	Epoxy Mastic Aluminum II	Phenicon HS Epoxy Phenicon Flake Filled Epo-Phen Nova-Plate UHS				

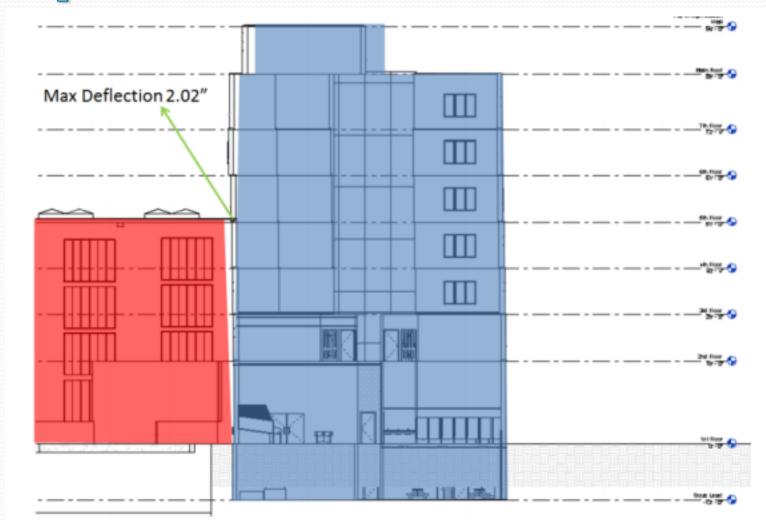
Epoxies—Common Problems and Most Probable Causes

		lost	Pro	bab	le C	aus	es																	-
Common Problems	Surface Contamination	Application Method	Exceeded Pot Life	High Humidity	Improper Hardener	Sweat-In Time	Recoat Time	Tirt Level	Improper Mix Ratio	UV Light Exposure	Absence of Light	Exposure to Chemicals	Wrong Reducer Solvent	Percent Reduction	Moisture/Condensation	Product Selection	Application Temperature	Surface Temperature	Initial Temperature 72 Hrs.	Film Thickness	Air Movement	Batch Variation	Primor	Surface Precaration
Discoloration/Yellowing			•	•	•	•			•	•	•	•			•	•	•	•	•		•			F
Color Variation				•	•	•		•	•	•	•	•			•	•	•	•	•		•	٠	•	Г
Blushing				•	•	•			•			•			•		•	•	•					
Uneven Gloss			•	•	•				•			•	•				•					•		
Exotherm (Hot Paint)			•		•				•								•							
Poor Intercoat Adhesion	•		•	•	•	•	•		•			•				•	•	٠	•	•			•	
Soft Film				•	٠	٠		•	•			•	•		٠		•	•		•	•			
Tacky Film/Slow Dry				٠	•	•		•	•				•		•		•	•		•	•			
Lifting/Wrinkling	•				•		•						•	•	•					•			•	
Bleeding	•						•	•								•							•	
Pinholing	•	•			•		•						•		•								-	
Cratering	•	•										•	•	•	٠								•	•
Low Film Thickness		•							•					•										
Sagging		•	•	٠			•						•	•		•	•		•		•			
Cracking/Crazing	•				•		٠		•	•														
Alligatoring	•																			•			•	

Image Courtesy of Sherwin Williams

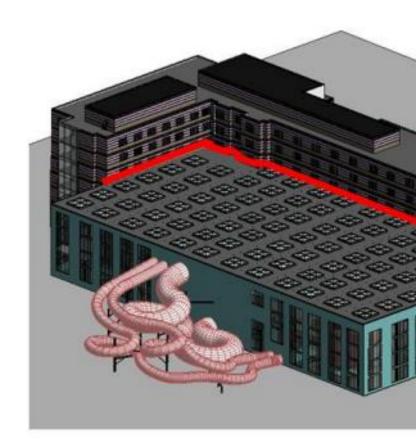


Expansion Joint:



APPEN

Expansion Joint Sizing									
Loading Case	Water Park ∆ (inch)	Hotel 5th Floor ∆ (inch)	Total deflection (inch)						
Case 1	0.7	0.66	1.36						
Case 2	1.51	0.51	2.02						
Case 3	0.4	1.07	1.47						
Case 4	1.01	0.8	1.81						
Seismic	1.06	0.66	1.72						



Expansion joint Location

